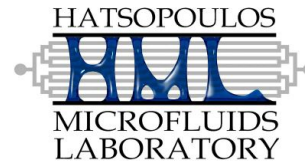


Rheological Fingerprinting of Complex Fluids and Soft Solids

Prof. Gareth H. McKinley

With Dr. Randy H. Ewoldt, Dr. Trevor Ng,
And Chris Dimitriou, Thomas Ober, Laura Casanellas

Department of Mechanical Engineering
Massachusetts Institute of Technology

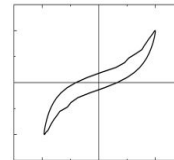


August 10, 2012

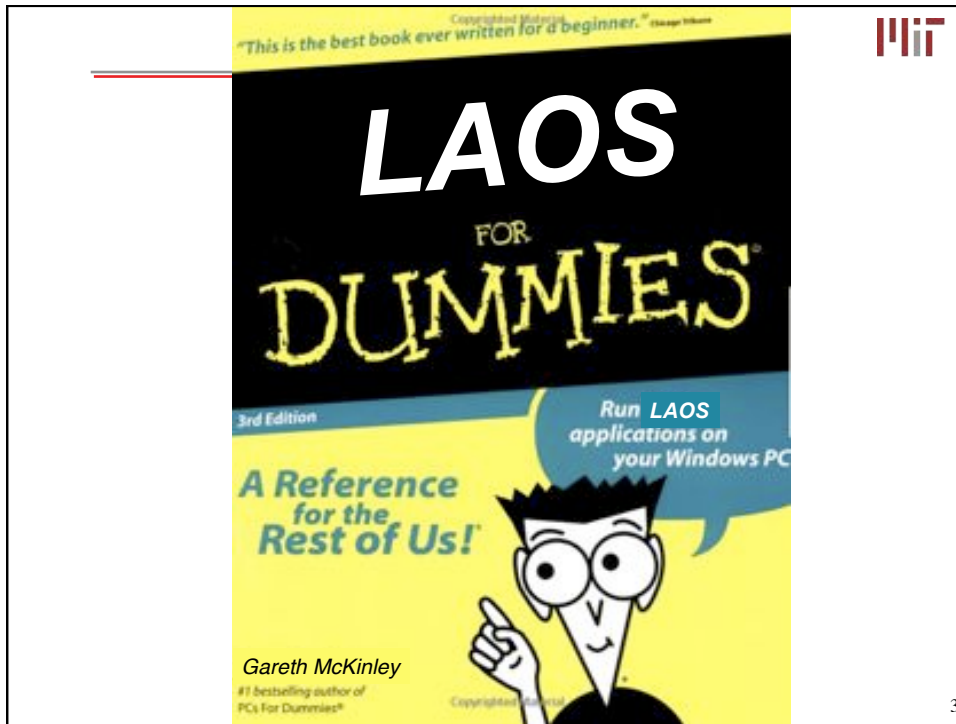
Outline



- **Rheological fingerprinting** of a complex fluid or soft solid
- **Large Amplitude Oscillatory Shear (LAOS)**
 - Useful ways to characterize nonlinear properties of complex fluids
 - How to quantify the measured response?
- **Wormlike Micellar Solutions**
 - Commonly used in shampoos/conditioners
 - Single mode linear viscoelastic response?
 - How do we characterize the nonlinear response?
- **The nonlinear rheology of snail slime**
 - How do we characterize the nonlinear response?
- **Connecting to Constitutive Models**
 - Extracting Constitutive parameters
- **What's Going on Inside**
 - Kinematics and Structural Probes
- **Yielding Materials; viscoelastoplasticity**
 - Carbopol Gels
 - LAOS for soft viscoelastic solids & gels
- **A mystery food (CSI; Lisbon)...**



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A review of nonlinear oscillatory shear tests: Analysis and application of large amplitude oscillatory shear (LAOS)

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ABSTRACT

Dynamic oscillatory shear tests are common in rheology and have been used to investigate a wide range of soft matter and complex fluids including polymer melts and solutions, block copolymers, biological macromolecules, polyelectrolytes, surfactants, suspensions, emulsions and beyond. More specifically, small amplitude oscillatory shear (SAOS) tests have become the canonical method for probing the linear viscoelastic properties of these complex fluids because of the firm theoretical background [1–4] and the ease of implementing suitable test protocols. However, in most processing operations the deformations can be large and rapid, it is therefore the nonlinear material properties that control the system

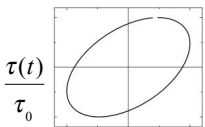
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Motivation for LAOS



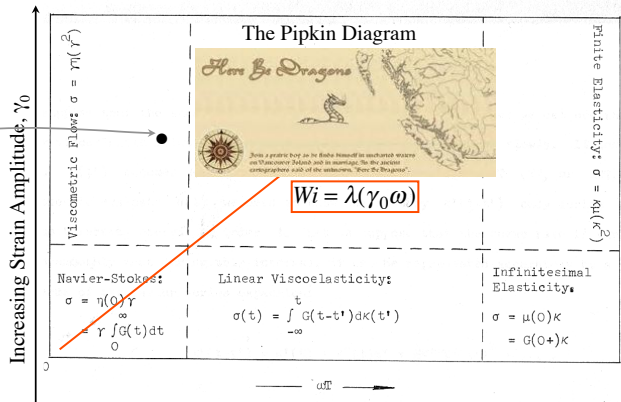
- Develop rheological methods that leverage the capabilities of modern instrumentation to probe the **nonlinear** properties of complex fluids and soft solids?
 - Foods and consumer products (gels, foams, surfactant systems)
 - gluten gel, micellar solutions, mucins, gastropod pedal mucus (snail slime)
- "... the whole infinite-dimensional space of shearing strain is projected onto two dimensions"
- "Nothing very systematic is known about the interior region..."

$\tau(t; \omega, \gamma_0)$



Bowditch-Lissajous Curve

The Pipkin Diagram




Increasing Strain Amplitude, γ_0

Increasing frequency, ω [rad/s], Deborah number, $\lambda\omega$

A.C. Pipkin, Lectures on Viscoelastic Theory, Springer, New York (1972)


Linear Viscoelasticity & Ellipses



- The equation for a linear viscoelastic response can be re-written (by eliminating time t) to show that the Lissajous figure for stress is **elliptical** when represented vs. shear strain or shear-rate.

$\gamma(t) = \gamma_0 \sin \omega t$

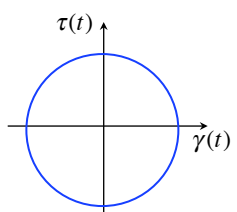
$\tau = \gamma_0 [G' \sin \omega t + G'' \cos \omega t]$



Jules Lissajous (1822-1880)

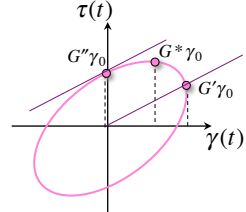
$$\tau^2 - 2G'\tau\gamma + \gamma^2(G'^2 + G''^2) = (G''\gamma_0)^2$$

Viscous dominated



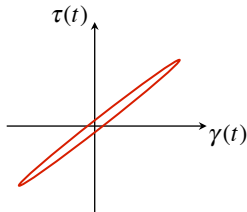
$\delta \rightarrow 90^\circ$

Viscoelastic



$90^\circ > \delta > 0^\circ$

elastic dominated



$\delta \rightarrow 0^\circ$

- For further reading, see Wikipedia, Wolfram Mathworld or <http://ibiblio.org/e-notes/Lis/Lissa.htm>

Nathaniel Bowditch (1773-1838)



- “I have now traced the mathematical analysis and experimental illustration of the Lissajous curves from France to Gt. Britain...to their home in Salem, MA. **The so-called Lissajous curves are the Bowditch curves**...They will continue, probably to be called the Lissajous curves. But their history should be known and will be known; though it is not necessary for the reputation of the self-taught mathematician, Dr. Nathaniel Bowditch”...

J. Lovering, Hollis Prof. of Physics, Harvard College “Anticipation of the Lissajous Curves”, Proc. Am. Acad. Arts & Sci. **16** (1881).

- Originally published in N. Bowditch, *Mem. Am. Acad. Arts. Sci* **3**, 413-436 (1815)

http://en.wikipedia.org/wiki/Nathaniel_Bowditch

In 1787, aged fourteen, Bowditch began to study algebra and two years later he taught himself calculus. He also taught himself Latin in 1790 and French in 1792 so he was able to read mathematic works such as Isaac Newton's *Philosophiae Naturae Principia Mathematica*. At seventeen, he wrote a letter to a Harvard University professor pointing out an error in the *Principia*....

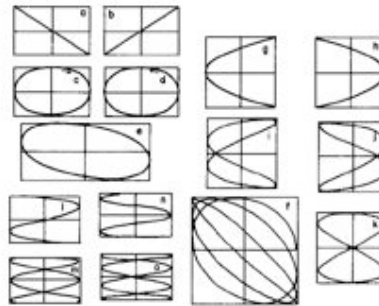


Fig. 3. Tracings of drawings of the orbits of two mutually orthogonal oscillations, published by N. Bowditch (Ref. 3). Drawings a, b, c, and d
A.D. Crowell, *Am. J. Phys* 1981

Tools for Analyzing Nonlinear Oscillatory Rheology



- **Pipkin Space** Pipkin, 1972
- **Bowditch-Lissajous curves** W. Philippoff, *Trans Soc. Rheol.* **10**, 1964
Dealy & Wissbrun *Melt Processing* 1990; Giacomin & coworkers
- **Fourier Transform Rheology** Dodge & Kreiger, *Trans Soc Rheol* 1972;
Willhelm et al., *Macromol. Mater Eng.* 2002

Presentation of the Bingham Medal to
Wladimir Philippoff

E. B. BAGLEY, *Canadian Industries Limited, McMasterville, Canada*

The Bingham Medal of the Society of Rheology for 1962 was presented to Dr. Wladimir Philippoff of the Esso Research and Engineering Company, Linden, New Jersey, in recognition of his outstanding contributions to the phenomenological rheology of viscoelastic materials. His dedication to experimental rheology over a period of almost thirty years has been manifested by his broad interests in new phenomena, in a wide range of materials, and in methods of measurement. He recognizes the basic scientific principle that theory and experiment are mutually dependent—that theory without experiment and experiment without theory are equally sterile. Undismayed by



Curves Cho. Ahn et al.. *JoR* 2005

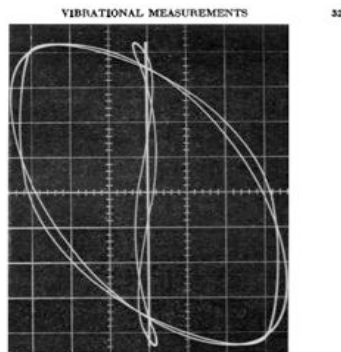



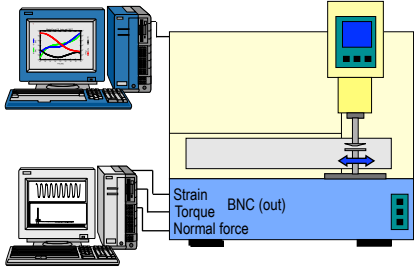
Fig. 4. Resolving the non-Newtonian recording into first and third harmonics with the electronic computer.

FT-Rheology and LAOS

The picture:



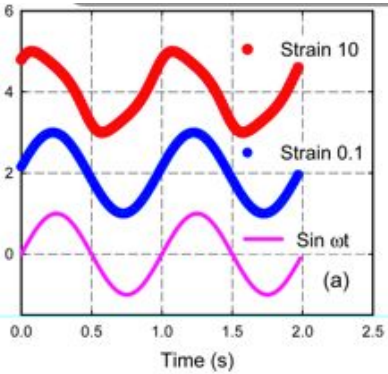
The set up:



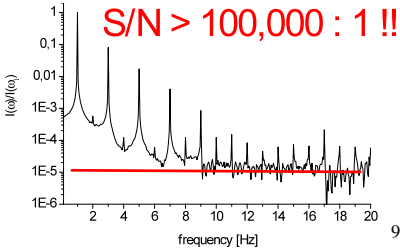
Strain
Torque
BNC (out)
Normal force

Ganeriwala & Rotz, *Polym. Eng. Sci.* **27** (1987)
M. Wilhelm; *Macromol. Mater. Eng.* **287** 83 (2002)

The data:



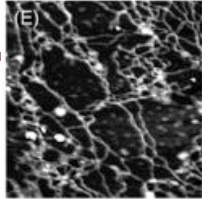
Time (s)



9

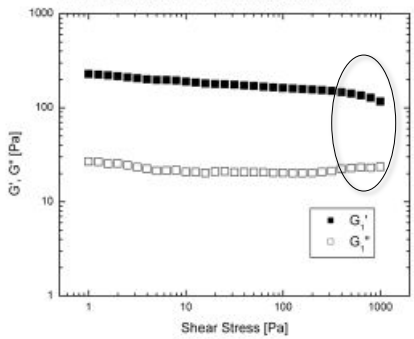
Linear Viscoelasticity of Mucin Gels

- The linear viscoelastic envelope is determined by performing an oscillatory stress sweep
- Elastic gel over a broad range of frequencies: $\xi \approx (k_B T / G')^{1/3} \approx 30\text{nm}$

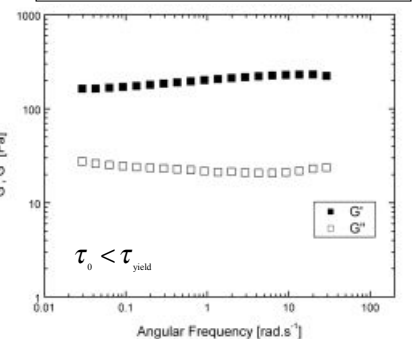


Miles & coworkers
Biophys. J., 2002


Probing for linear regime at 1 rad/s



Frequency sweep at 5 Pa stress amplitude



$\tau_0 < \tau_{\text{yield}}$



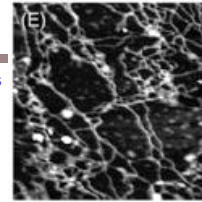
$$\tau_y \approx \frac{Mg}{A_{\text{contact}}} \sim 100 - 200 \text{ Pa}$$

2cm steel plate, T=22°C, 200µm gap

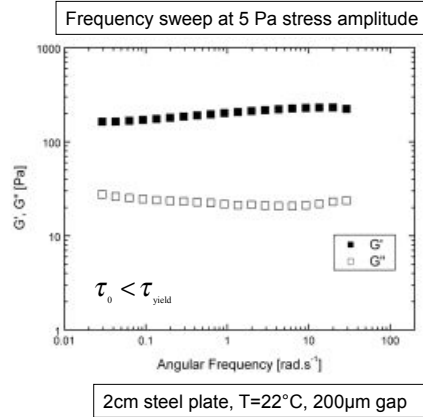
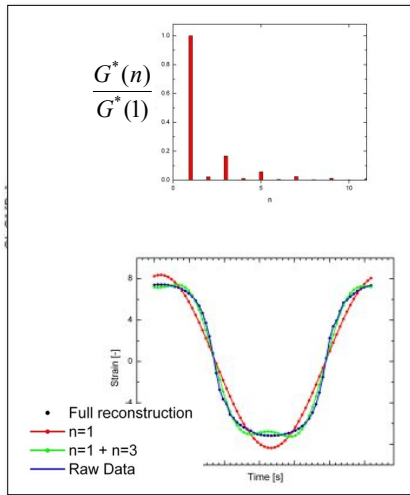
Ewoldt, Clasen, GHM; *Soft Matter* 2007 10

Linear Viscoelasticity of Mucin Gels

Miles & coworkers
Biophys. J., 2002



- The linear viscoelastic envelope is determined by performing an oscillatory stress sweep
- Elastic gel over a broad range of frequencies: $\xi \approx (k_B T / G')^{1/3} \approx 30 \text{ nm}$



Ewoldt, Clasen, GHM; *Soft Matter* 2007 11

Physical Interpretation of LAOS Deformations



- General Fourier decomposition $\tau = \gamma_0 \sum_{n \text{ odd}} G_n'' \cos(n\omega t) + G_n' \sin(n\omega t)$

A New Approach

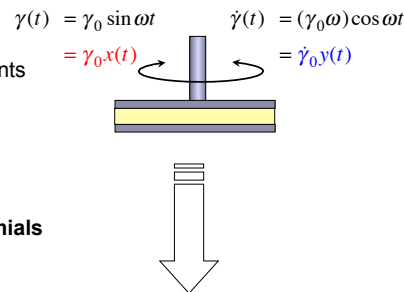
- Consider strain and strain rate as independent *orthogonal* inputs

Cho, Hyun, Ahn, Lee, *J. Rheol.* 49 (2005).

- Decompose output stress using symmetry arguments into 'elastic' (x) and 'viscous' (y) contributions

- Point group symmetries & Frieze group analysis
Rogers & Vlassopoulos, *J. Rheol.* 54 (2010).

- Represent the unknown material response or *Transfer Function* in terms of **Chebyshev polynomials** in x and y:



$$\tau(t; \omega, \gamma_0) \equiv \tau_{elastic}(\gamma(t)) + \tau_{viscous}(\dot{\gamma}(t)) = \gamma_0 \sum_{i=1}^N e_i T_i(x) + \gamma_0 \omega \sum_{i=1}^N v_i T_i(y)$$

R.H. Ewoldt, A.E. Hosoi, GHM, *J. Rheology* 52 (2008)

12

The Benefits of Chebyshev* polynomials

$$\tau(t; \omega, \gamma_0) \equiv \tau_{elastic}(\gamma(t)) + \tau_{viscous}(\dot{\gamma}(t)) = \gamma_0 \sum_{i=1}^N e_i T_i(x) + \gamma_0 \omega \sum_{i=1}^N v_i T_i(y)$$

mathworld.wolfram.com

$T_0(x) = 1$
 $T_1(x) = x$
 $T_2(x) = 2x^2 - 1$
 $T_3(x) = 4x^3 - 3x$
 $T_4(x) = 8x^4 - 8x^2 + 1$
 $T_5(x) = 16x^5 - 20x^3 + 5x$

BENEFITS

- Chebyshev polynomials are *orthonormal* and offer near-optimal polynomial interpolation
- The **Chebyshev coefficients** (v_i & e_i) have physical interpretations with respect to familiar rheological concepts such as *shear-thinning* and *strain-stiffening*
- Temporal response can always be reconstructed using identities for Chebyshev polynomials

$T_i(x) \equiv T_i(\sin \omega t) = (-1)^{i+1} \sin(i\omega t)$
 $T_i(y) \equiv T_i(\cos \omega t) = \cos(i\omega t)$

Example: $T_3(\cos z) \equiv \cos 3z = 4 \cos^3 z - 3 \cos z$
 ($i=3; z = \omega t$)

* Also transliterated as *Tschebychev*
 * PhD Students of Tschebychev include Markov, Lyapunov...

Example: Nonlinear Elastic Solid

- LAOS for nonlinear elastic solid
 - Strain-stiffening modulus: $\tau = G(\gamma)\gamma$
- Higher order terms are mutually orthogonal...

Chebyshev Decomposition

$\tau_{elastic} = \gamma_0 \sum_{i=1}^N e_i T_i(x)$

Material Moduli:

$$e_1 = G'_1 = g_1 + \frac{3}{4} \left(\frac{\gamma_0}{\gamma^*} \right)^2 g_3$$

Linear elastic limit

$$e_3 = -G'_3 = + \frac{1}{4} \left(\frac{\gamma_0}{\gamma^*} \right)^2 g_3$$

Direct measure of the nonlinearity

Additional Physical Quantifiers of Nonlinearity

Strain-stiffening index, S

- G'_M : small-strain (tangent) modulus
- G'_L : large-strain (secant) modulus

$$G'_M = \left. \frac{d\tau}{d\gamma} \right|_{\gamma=0} = e_1 - 3e_3 + 5e_5 + \dots = \sum_{n=odd} nG'_n$$

$$G'_L = \left. \frac{\tau}{\gamma} \right|_{\gamma=\gamma_0} = e_1 + e_3 + e_5 + \dots = \sum_{n=odd} G'_n (-1)^{(n-1)/2}$$

$$S = \frac{G'_L - G'_M}{G'_L} = 1 - \frac{\sum_{n=odd} nG'_n}{\sum_{n=odd} G'_n (-1)^{(n-1)/2}} = \frac{4e_3 \dots}{e_1 - 3e_3 + 5e_5 \dots}$$

- $S = 0$ for linear viscoelastic material
- $S < 0$ for strain softening
- $S > 0$ for strain stiffening

Ewoldt, Hosoi, GHM; *J. Rheol.* 2008 15

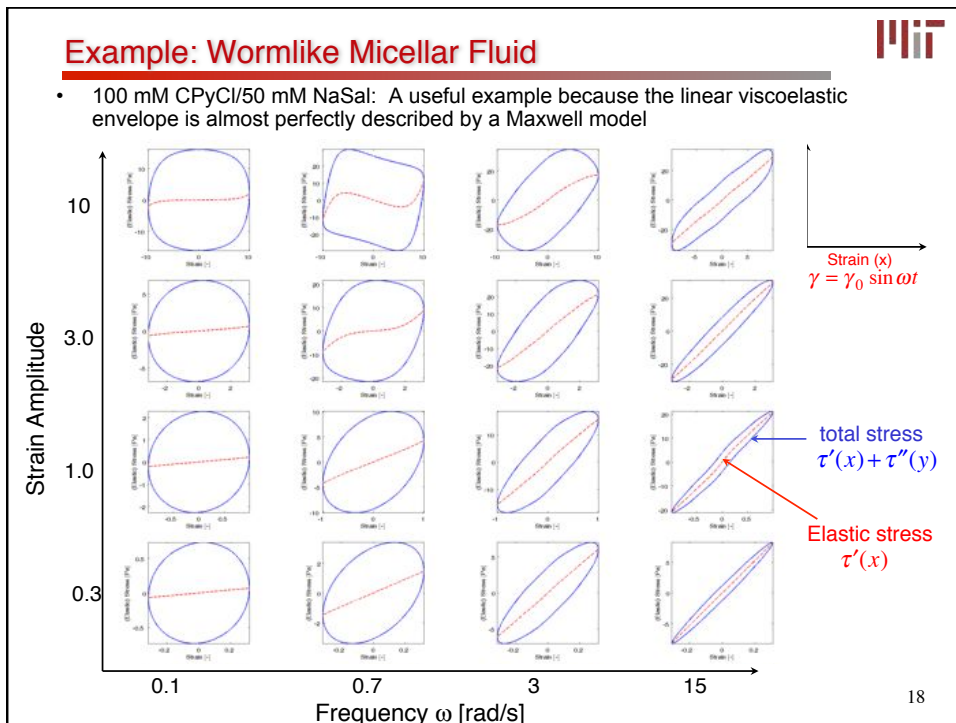
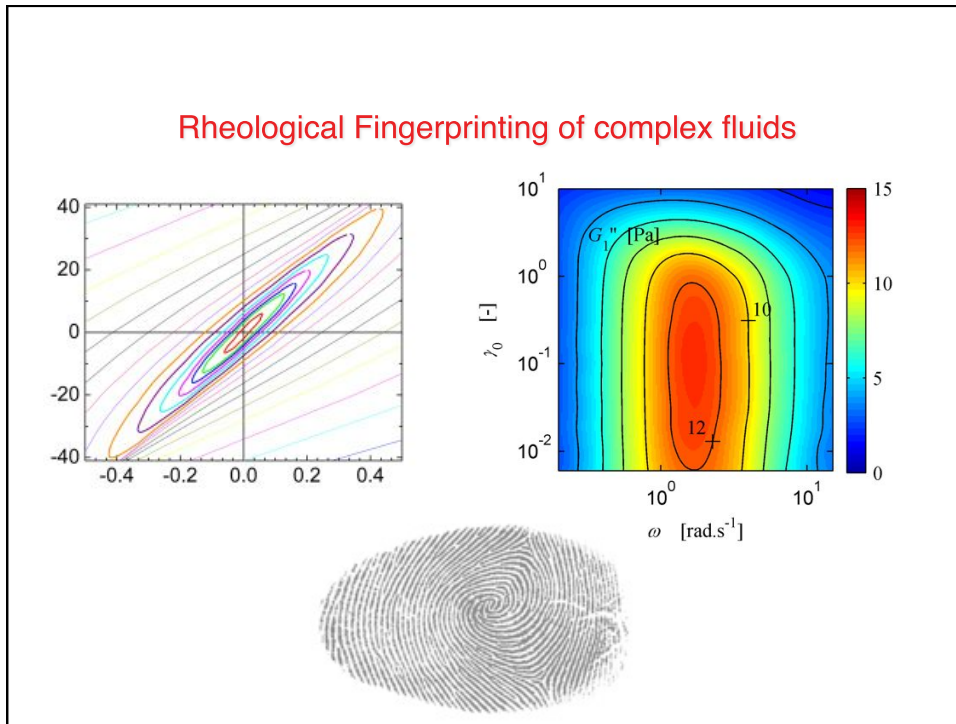
Example: Evaluating Measures of Nonlinear Moduli

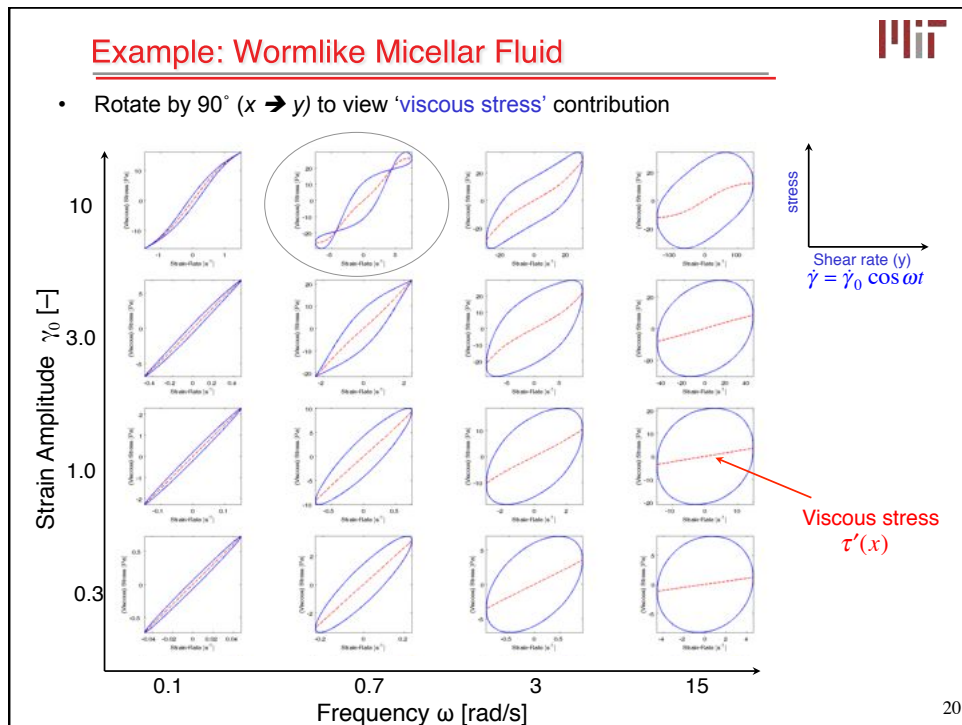
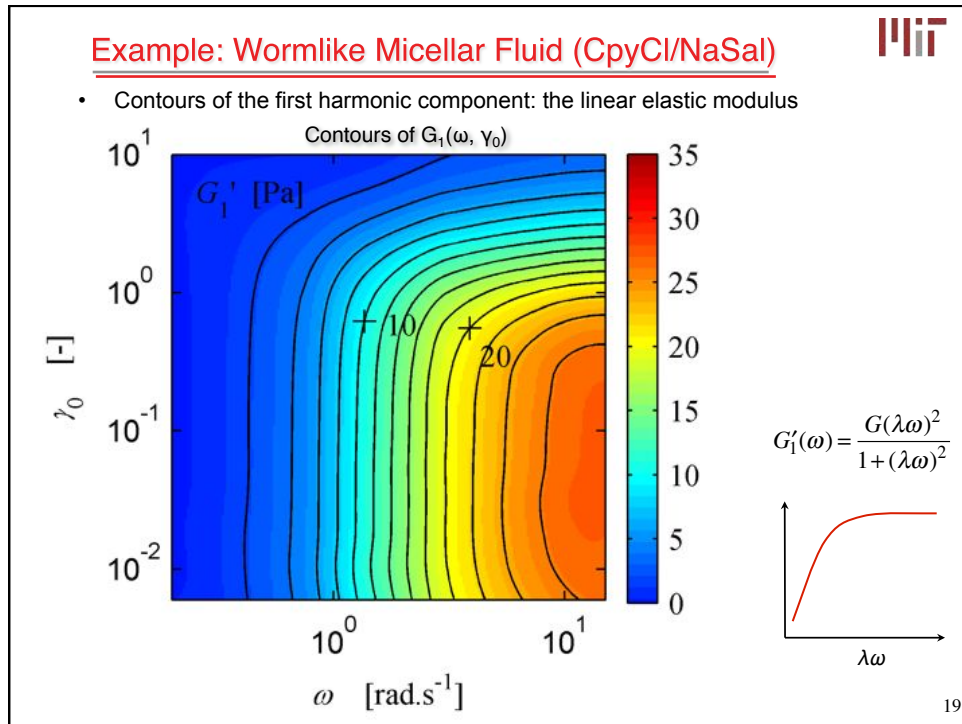
(a) Linear viscoelastic

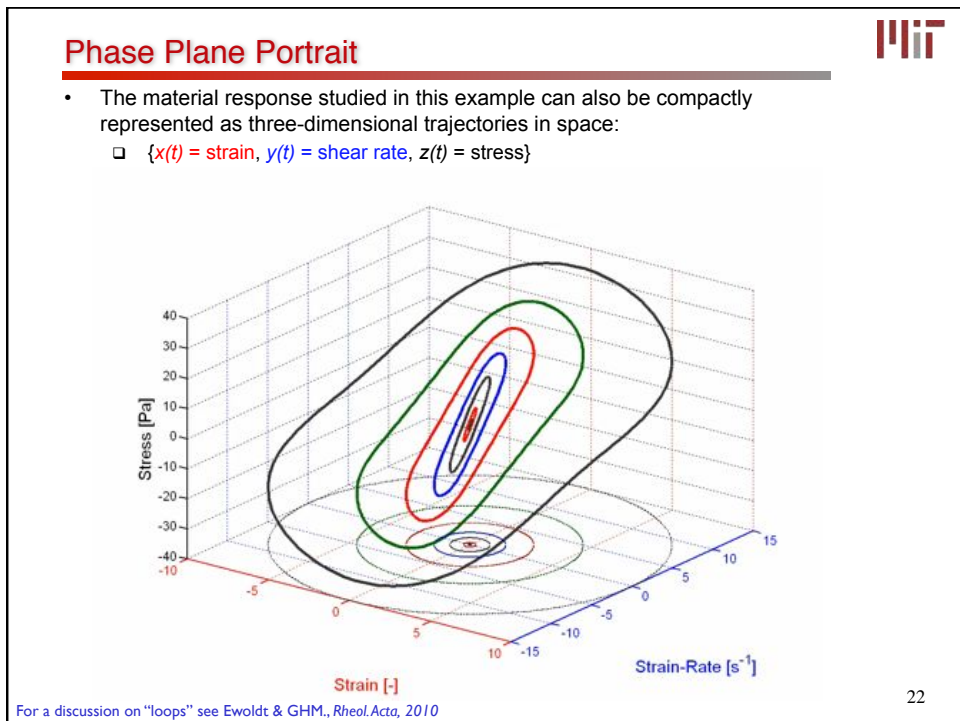
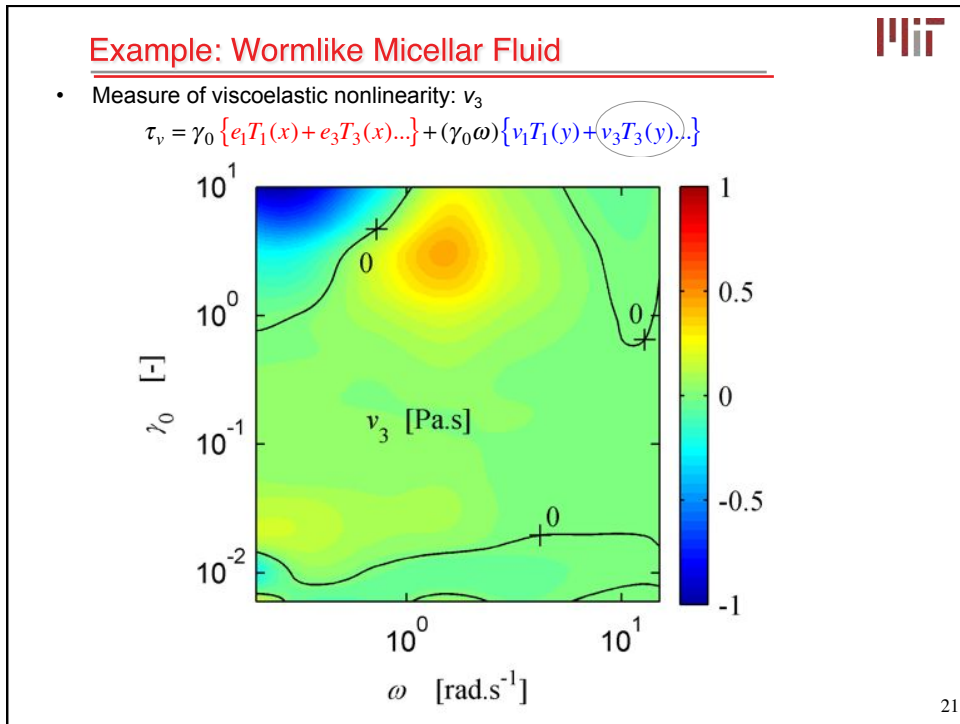
(b) Nonlinear viscoelastic

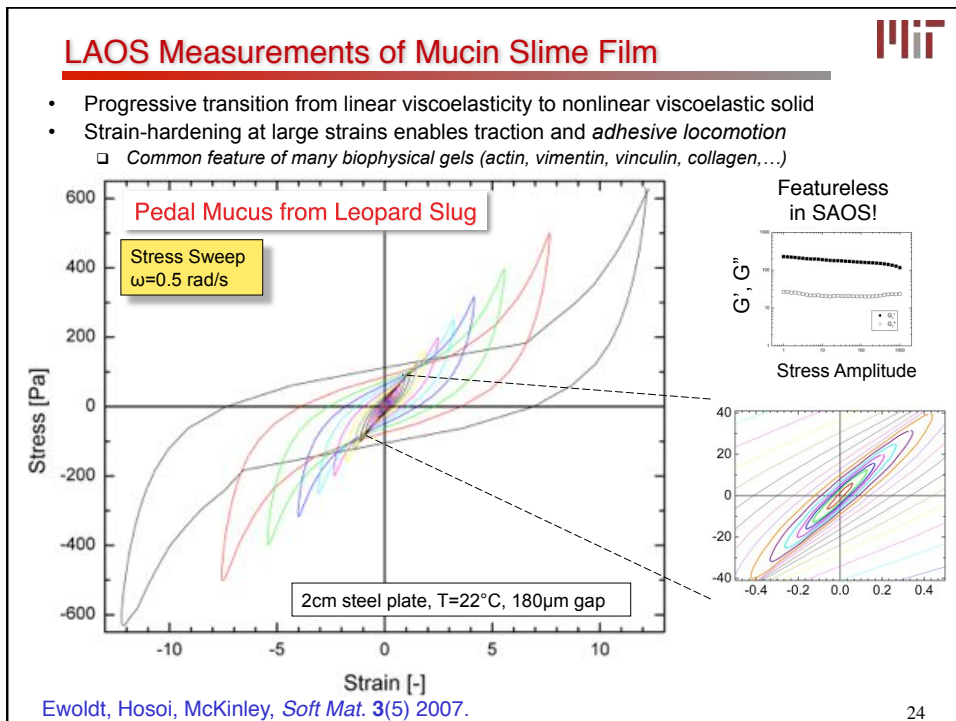
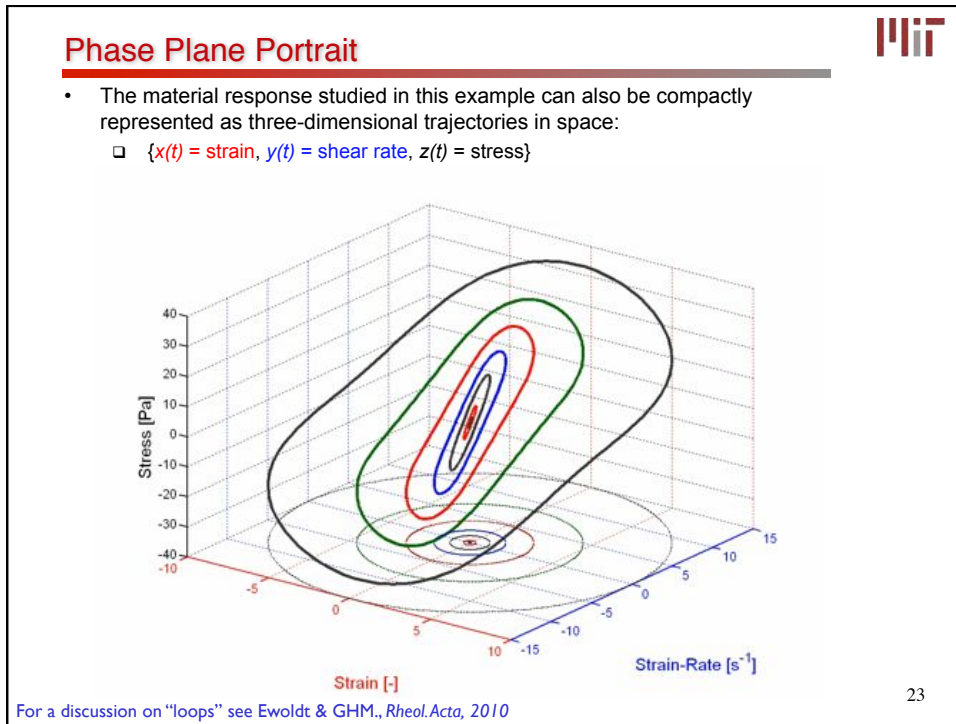
| | $\gamma_0 = 0.5$ | | $\gamma_0 = 3.2$ | |
|---|------------------|-----------------------|------------------|----------------------------------|
| Snail Pedal Mucus Roughened Plates T = 25°C | 123 | G'_e [Pa] | 121 | (prior standard) |
| | 121 | G'_M [Pa] | 59.1 | tangent, minimum strain |
| | 123 | G'_L [Pa] | 157 | secant, large strain |
| | 122 | G'_K [Pa] | 580 | tangent, large strain |
| | +0.4% | $e_3 / e_1 * 100$ [%] | +23.8% | intra-cycle elastic nonlinearity |

Ewoldt, Hosoi, GHM; *J. Int. Comp. Biol.* 2009









Using LAOS to Evaluate Constitutive Models



- Use LAOS fingerprints to evaluate nonlinear coefficients of constitutive models for complex fluids and compare with experiments

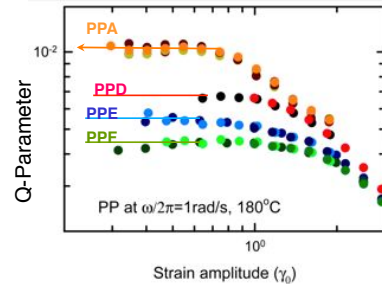
□ The Q-Parameter (Hyun, Wilhelm)

$$\lim_{\gamma_0 \rightarrow 0} \frac{I_3}{I_1} \equiv \lim_{\gamma_0 \rightarrow 0} I_{3/1} = Q(\omega)\gamma_0^2 + O(\gamma_0^4) \dots$$

Remember: $\sin x \approx x - \frac{1}{3}x^3 \dots \Rightarrow I_{3/1} \sim x^2$

□ Loss of phase information... (also have to monitor phase angle δ_3)

$$\frac{I_3}{I_1} = \frac{\sqrt{e_3^2 + (v_3\omega)^2}}{\sqrt{e_1^2 + (v_1\omega)^2}}$$



Commercial PP (linear chain structure)

| Sample | Mn | Mw | MWD | Structure |
|--------|------|------|-----|-----------|
| PP-A | 106k | 460k | 4.3 | Linear |
| PP-D | 37k | 270k | 7.3 | Linear |
| PP-E | 50k | 240k | 4.8 | Linear |
| PP-F | 57k | 230k | 4 | Linear |
| PP-G | 76k | 220k | 3.9 | Linear |

- Other general representations of linear and nonlinear viscoelastic response: $R'(\omega, \gamma_0)$, $R''(\omega, \gamma_0)$ (Rogers, JoR 56(5), 2012)

K. Hyun, M. Wilhelm; *Macromolecules* 42 411 (2009) 25

The Reptation Model in LAOS



Behavior of Concentrated Polystyrene Solutions in Large-Amplitude Oscillating Shear Fields

DALE S. PEARSON and WILLIE E. ROCHEFORT, *Bell Laboratories, Murray Hill, New Jersey 07974*

$$\sigma_{xy}(t) = \gamma_0 [G'_{11}(\omega) \sin \omega t + G''_{11} \cos \omega t] + \gamma_0^2 [G'_{31}(\omega) \sin \omega t + G''_{31} \cos \omega t + G'_{33}(\omega) \sin 3\omega t + G''_{33} \cos 3\omega t] + O(\gamma_0^3) \quad (14)$$

where

$$G'_{31} = -\frac{3}{14} \frac{\rho k T}{N_e} \sum_{p, \text{odd}} \frac{8}{\pi^2 p^2} \left(\frac{2\omega^2 \tau_d^2}{p^4 + \omega^2 \tau_d^2} - \frac{2\omega^2 \tau_d^2}{p^4 + 4\omega^2 \tau_d^2} \right) \quad (15a)$$

$$G''_{31} = -\frac{3}{14} \frac{\rho k T}{N_e} \sum_{p, \text{odd}} \frac{8}{\pi^2} \left(\frac{\omega \tau_d}{p^4 + \omega^2 \tau_d^2} - \frac{\omega \tau_d}{p^4 + 4\omega^2 \tau_d^2} \right) \quad (15b)$$

$$G'_{33} = \frac{3}{28} \frac{\rho k T}{N_e} \sum_{p, \text{odd}} \frac{8}{\pi^2 p^2} \left(\frac{\omega^2 \tau_d^2}{p^4 + \omega^2 \tau_d^2} - \frac{4\omega^2 \tau_d^2}{p^4 + 4\omega^2 \tau_d^2} + \frac{3\omega^2 \tau_d^2}{p^4 + 9\omega^2 \tau_d^2} \right) \quad (16a)$$

$$G''_{33} = \frac{3}{28} \frac{\rho k T}{N_e} \sum_{p, \text{odd}} \frac{8}{\pi^2} \left(\frac{\omega \tau_d}{p^4 + \omega^2 \tau_d^2} - \frac{2\omega \tau_d}{p^4 + 4\omega^2 \tau_d^2} + \frac{\omega \tau_d}{p^4 + 9\omega^2 \tau_d^2} \right) \quad (16b)$$

All the sums in these equations can be evaluated, leaving analytical expressions for G'_{31} and G'_{33} (see Appendix A).



(a)



(b)



(c)

Journal of Polymer Science: Polymer Physics Edition, Vol. 20, 83-98 (1982); © 1982 John Wiley & Sons, Inc. CCC 0098-1273

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The Reptation Model in LAOS

- Evaluating the Q parameter for the DE model gives:

$$\lim_{\omega \rightarrow 0} Q_0(\omega) = \frac{1}{3} (\lambda_d \omega)^2$$

Reptation time

| | M_b | M_a |
|------|-------|-------|
| 76K | 75.9 | - |
| 100K | 100 | - |
| 220K | 214 | - |
| 330K | 330 | - |
| C632 | 275 | 25.7 |
| C622 | 275 | 11.7 |
| C642 | 275 | 47 |

Effect of Chain-Branching on Nonlinearity in LAOS

□ Comb PS with **entangled branches** displays **two relaxation processes**, one corresponding to **the branches'** disentanglements and one due to the **backbone chain**.

K. Hyun, M. Wilhelm; *Macromolecules* 42 411 (2009)
K. Hyun et al. *Prog Polym Phys.* (2011)

Comparison of LAOS Data with MSF Model

- Molecular Stress Function model of M.H. Wagner & coworkers

Chain orientation
Chain stretching

$$I_{3/1} = \frac{|G_{33}^*|}{|G_{11}^*|} \gamma_0^2 \propto (\alpha - \beta) \gamma_0^2$$

$$\lim_{\omega \rightarrow 0} Q_0(\omega) = \frac{3}{2} (\alpha - \beta) (\lambda_d \omega)^2$$

α = 5/21 : Doi-Edwards; IAA

β = 1/5 : Quadratic MSF

Moderate Amplitude Oscillatory Shear (MAOS)!
M. H. Wagner, et al.; *J. Rheol.* 55 495 (2011)

Fluids with Yield Stresses/Critical Stresses MIT

How "yield-stressy" is a given fluid?


Most common rheometric tests

- Steady flow: steady state nonlinear viscous properties $\eta(\dot{\gamma})$
- Thixotropic loops: time-dependent viscous properties $\eta(\dot{\gamma}_{up}), \eta(\dot{\gamma}_{down})$
- Linear viscoelasticity: $G'(\omega), G''(\omega)$

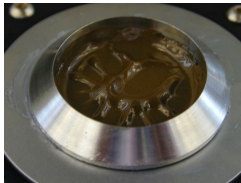
A more-complete characterization?

- Large amplitude oscillatory shear (LAOS) systematically spans the timescale and magnitudes of deformation
- Probes time-dependent nonlinear viscous *and* elastic properties
- Connects steady flow viscosity, linear viscoelastic moduli, and nonlinear viscoelastic properties

Carbopol Gel
W. Hart, P&G



Oil-based Drilling Mud (Invert Emulsion)
J. Maxey, Halliburton



Ewoldt, Winter, Maxey, McKinley, *Rheol. Acta.* **49**(2), 2010; Dimitriou et al., *JoR* 2012 submitted. 29

Stress-Controlled Experiments: LAOStress MIT

- For many foods and consumer products it is more common to perform stress-controlled experiments.
- LAOStress** is a great experimental methodology to probe differences between yielded/unyielded regime as well as limitations of constitutive models
- Decompose strain into an **elastic** component and a **viscoplastic** component
 - Describe in terms of models that naturally capture 'sequence of physical processes' for elastic strain, yielding, viscoplastic flow

Normalized Input sinusoidal stress: $x(t) = \frac{\tau(t)}{\tau_0} = \cos \omega t$

Fourier series representation of strain:

$$\gamma(t) = \tau_0 \sum_{n \text{ odd}} J'_n \cos n\omega t + J''_n \sin n\omega t$$

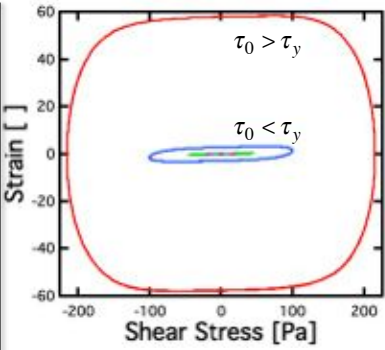
Chebyshev representation:

$$\gamma_e(t) = \tau_0 \sum_{n \text{ odd}} J'_n \cos n\omega t = \tau_0 \sum_{n \text{ odd}} c_n T_n(x)$$

compliances

$$\dot{\gamma}_p(t) = -\tau_0 \sum_{n \text{ odd}} n\omega J''_n \cos n\omega t = \tau_0 \sum_{n \text{ odd}} \phi_n T_n(x)$$

Fluidities



Lauger & Stettin, *Rheol. Acta* 2010
S. Rogers & coworkers, *J. Rheol.* 2011, 12 30

The Basic Anatomy of a Lissajous Figure in LAOStress MIT

- Input is an oscillating stress field $\tau(t; \omega) = \tau_0 \cos \omega t \Rightarrow$ output is the strain
- Shear strain and shear rate are no longer orthogonal variables
- How do I traverse this trajectory in 3-dimensional space?
- How do I describe it quantitatively?

$\gamma(t; \omega, \tau_0)$

The Bingham Model in LAOS

Ewoldt, Winter, Maxeey, GHM, *Rheol. Acta.* **49**(2), 2010; Dimitriou et al., *JOR* 2012 submitted. 31

Graphical Definitions of Nonlinear Compliances MIT

Linear regime $\tau < \tau_y$

Nonlinear regime $\tau > \tau_y$

Nonlinear compliance measure: (non-locally computed!)


$J'_M = \left. \frac{d\gamma}{d\tau} \right|_{\tau=0} = c_1 - 3c_3 + 5c_5 \dots$

| | $\tau_0 = 4 \text{ Pa}$ | | $\tau_0 = 100 \text{ Pa}$ |
|----------------------|---------------------------------|--|---------------------------|
| 2.9×10^{-3} | $J'_1 \text{ (Pa}^{-1}\text{)}$ | | 5.7×10^{-3} |
| 2.9×10^{-3} | $J'_M \text{ (Pa}^{-1}\text{)}$ | | 7.0×10^{-3} |
| 2.9×10^{-3} | $J'_L \text{ (Pa}^{-1}\text{)}$ | | 13.9×10^{-3} |

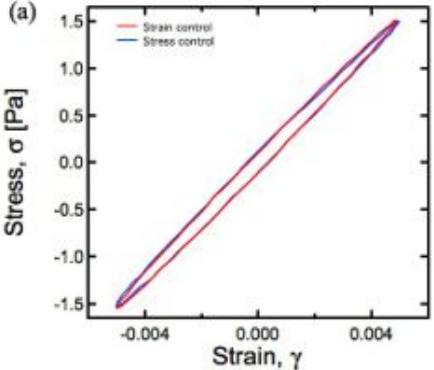
- For yielding materials, elastic LAOStress measures are typically more effective at quantifying nonlinear elastic behavior
- Typical yielding material retain some (measurable) elasticity even under flow

Lauger & Stettin, *Rheol. Acta* 2010; Dimitriou et al., *JOR* 2012 32

LAOStress vs. LAOStrain

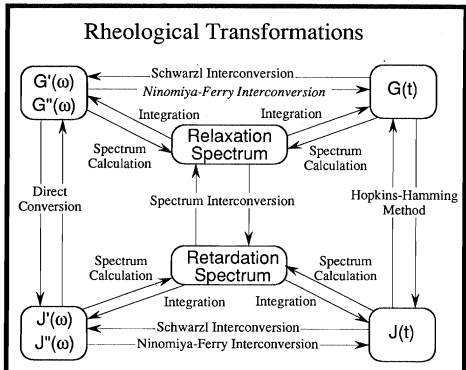


- In the linear regime the two techniques yield the same information
 - Linear viscoelastic moduli and compliances are interchangeable $G^*(\omega) J^*(\omega) = 1$



(a)

Rheological Transformations




J. D. Ferry, Viscoelastic Properties of Polymers (1980)

- Energy dissipated in cycle (per unit volume) is always represented by area enclosed by the corresponding Bowditch-Lissajous curve:

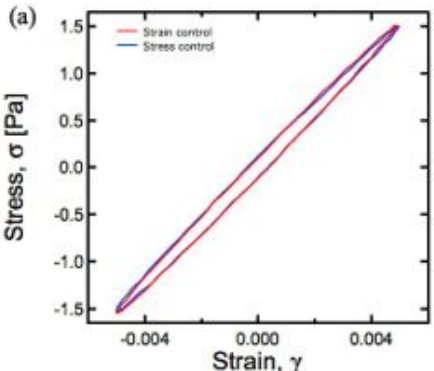
$$E_d = \oint \tau(t) \dot{\gamma}(t) dt$$

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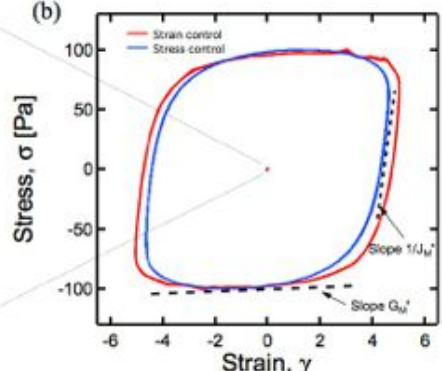
LAOStress vs. LAOStrain



- In the linear regime the two techniques yield the same information
 - Linear viscoelastic moduli and compliances are interchangeable $G^*(\omega) J^*(\omega) = 1$
 - ...this is NOT true in the nonlinear regime!



(a)




(b)

- Energy dissipated in cycle (per unit volume) is always represented by area enclosed by the corresponding Bowditch-Lissajous curve:

$$E_d = \oint \tau(t) \dot{\gamma}(t) dt$$

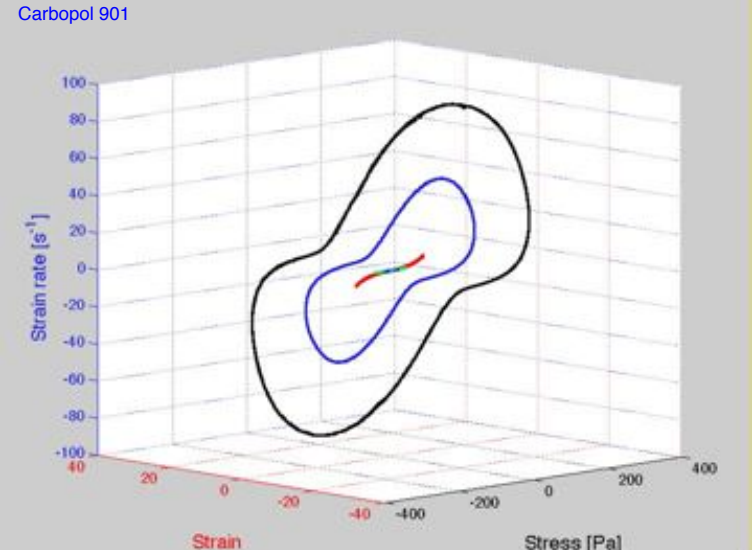
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LAOStress: Yielding in Three-Dimensions




- Visualize the yielding surface as a function of stress amplitude and frequency
 - Remember shear strain and shear rate are no longer orthogonal!

Carbopol 901

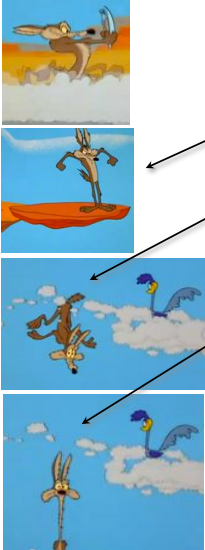
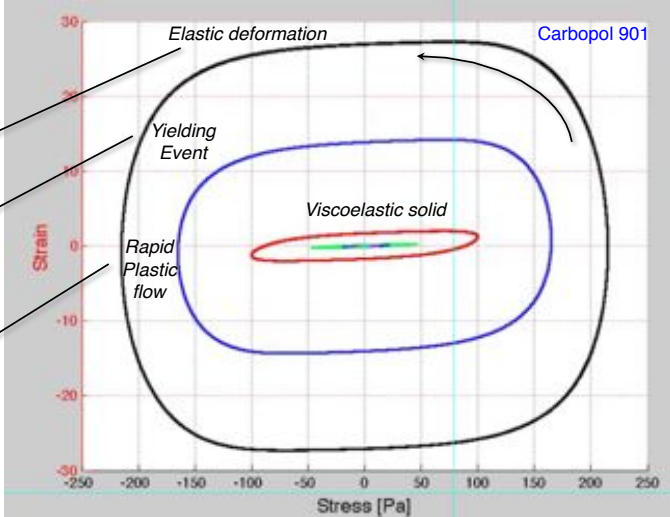


35

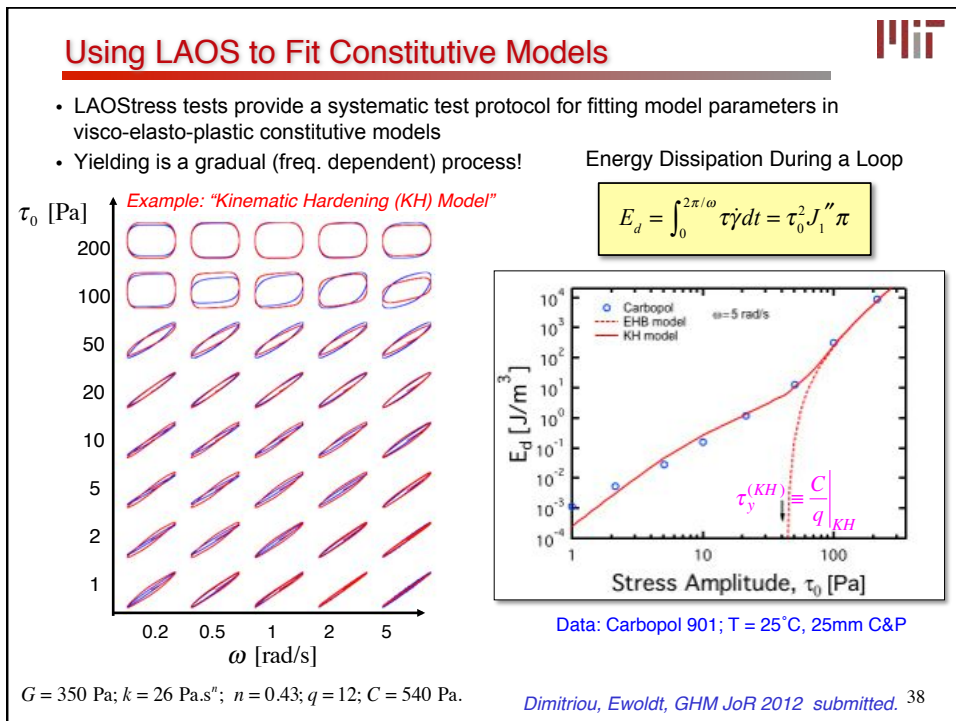
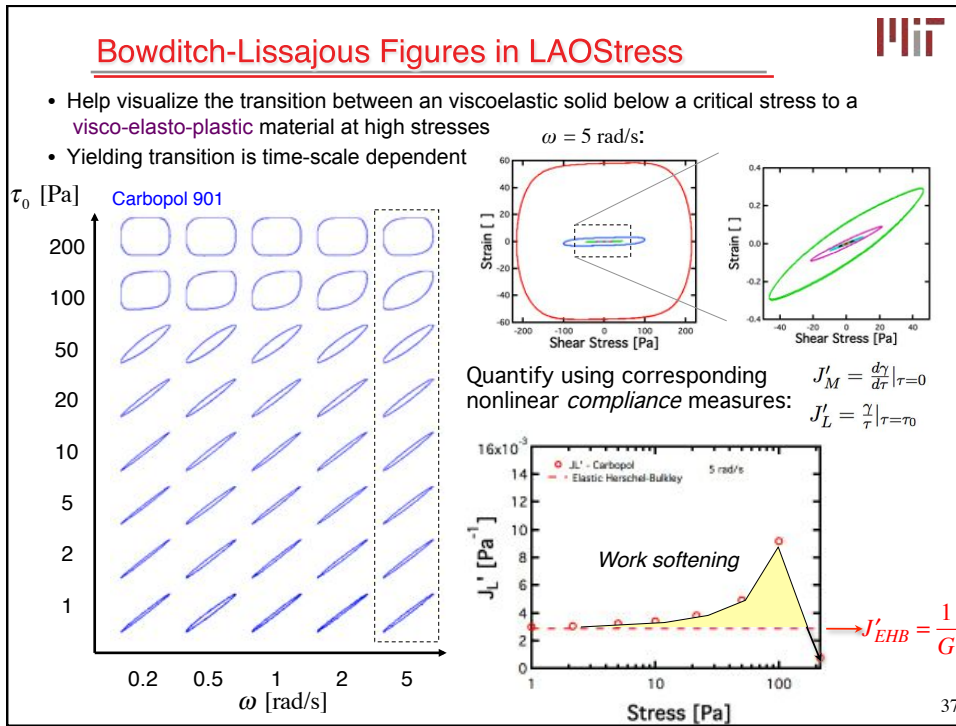
LAOStress: Yielding Signature in a Lissajous Figure




- Visualize the yielding surface as a function of stress amplitude and frequency
 - Also: remember shear strain and shear rate are no longer orthogonal!





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What's Going On Inside?





In-Situ Rheo-PIV, Rheo-PTV, Rheo-NMR, Ultrasound...

- Validate the assumption of homogeneous shearing flow
- Investigate slip at boundaries
- Investigate internal fracture/"shear-banding"

Rheo-SANS, Rheo-XRAY...

- Investigate deformation of microstructure and compare with microstructural models
- Mapping of local concentration variations under imposed steady shear

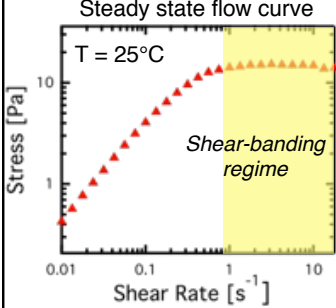
Challenge: achieve temporal and spatial resolution of oscillatory flow dynamics...

Example: Model Entangled Worm-like Micellar Fluid (CPyCl/NaSal) in LAOS

Rehage & Hoffmann, [Molecular Physics](#), 74(5): 933-973 (1991) 39


Steady state flow curve

T = 25°C



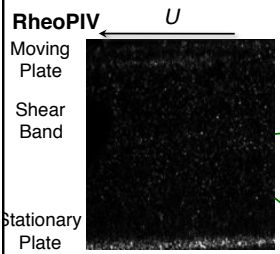
Shear-banding regime

Pipkin Diagram for LAOS of a Shear-Banding Material

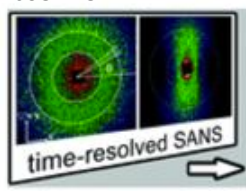


- Constitutive Modeling:
 - Rolie-Poly Model for monodisperse entangled polymer melts; [Adams, Fielding, Olmsted](#)
 - Two-species VCM model, (& Larson PEC model) for micellar networks; [Zhou, Cook, GHM](#)

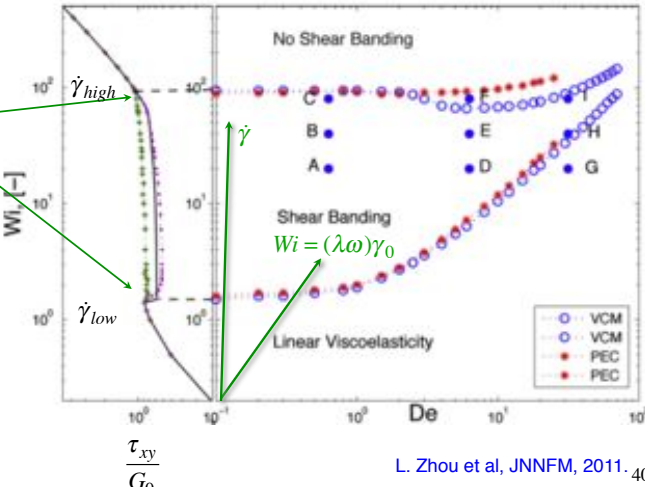
RheoPIV



RheoSANS




Rogers, Kohlbrecher, Lettinga, [Soft Matter](#) 8 (2012)



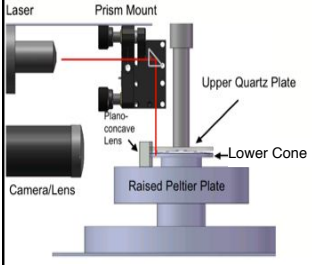
L. Zhou et al, [JNNFM](#), 2011. 40

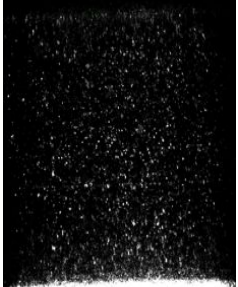
Rheo-PIV of WLM in Oscillatory Shear

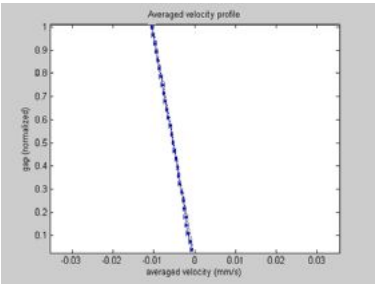


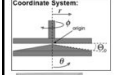
- In SAOS velocity gradient field is homogeneous as expected

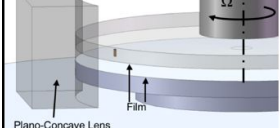
Small strain amplitude ($\gamma_0 = 10\%$): $v_x(y,t) = \gamma_0 \omega (y/H) \cos \omega t$



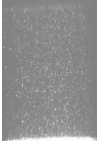


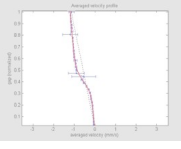







Large strain amplitude ($\gamma_0 = 500\%$):






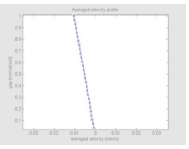
[Dimitriou et al. Energy & Fuels, 25, 2012](#)
[Dimitriou et al. Rheol. Acta. 51\(5\), 2012](#)¹

Rheo-PIV of WLM in Oscillatory Shear



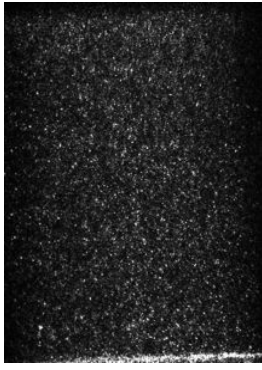
Small strain amplitude ($\gamma_0 = 10\%$):

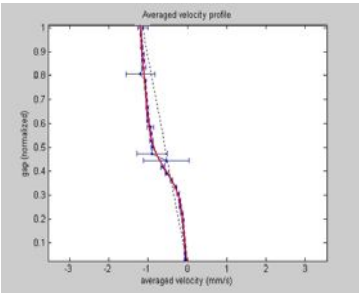




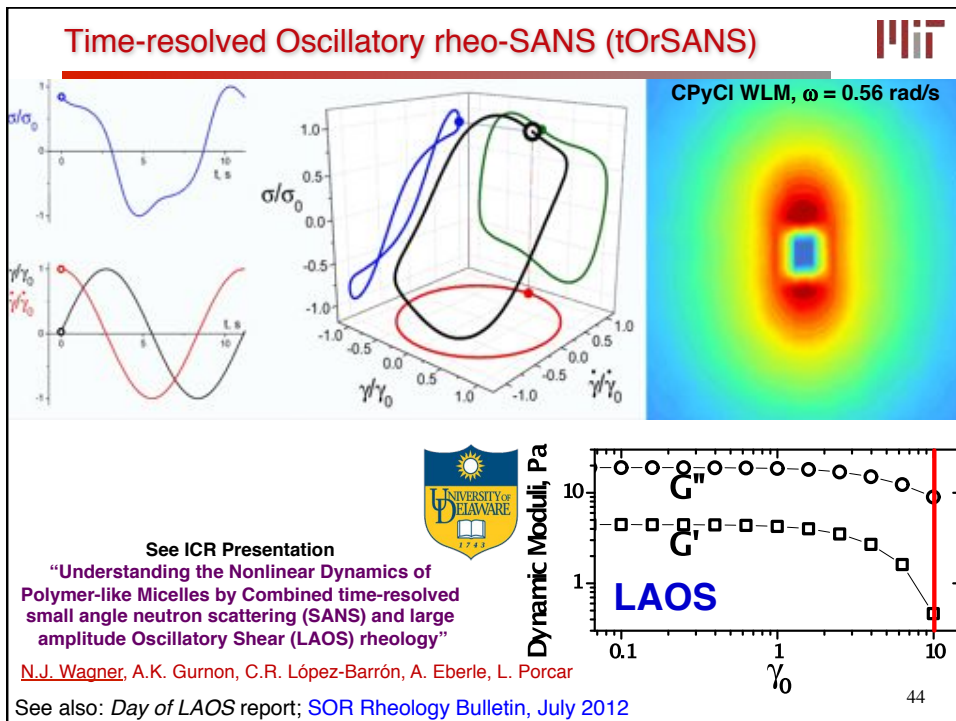
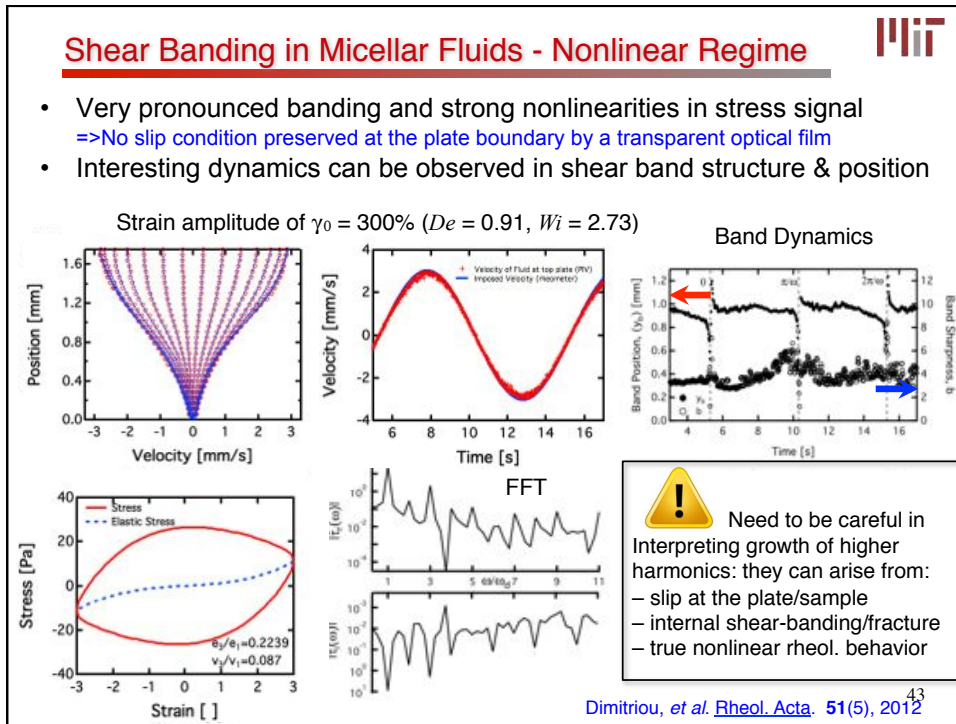
- In LAOS the velocity profile exhibits a kink in the center of the gap

Large strain amplitude ($\gamma_0 = 500\%$):





[Dimitriou et al. Rheol. Acta. 51\(5\), 2012](#)²



CSI: Lisbon













* CSI = Controlled Stress Investigation


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CSI: Lisbon




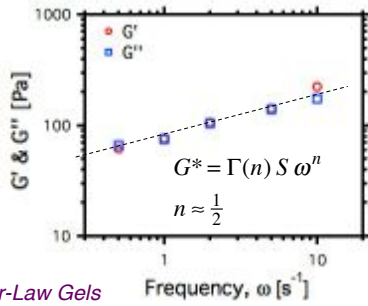
Queijo da Serra!



This cheese traveled a long way...



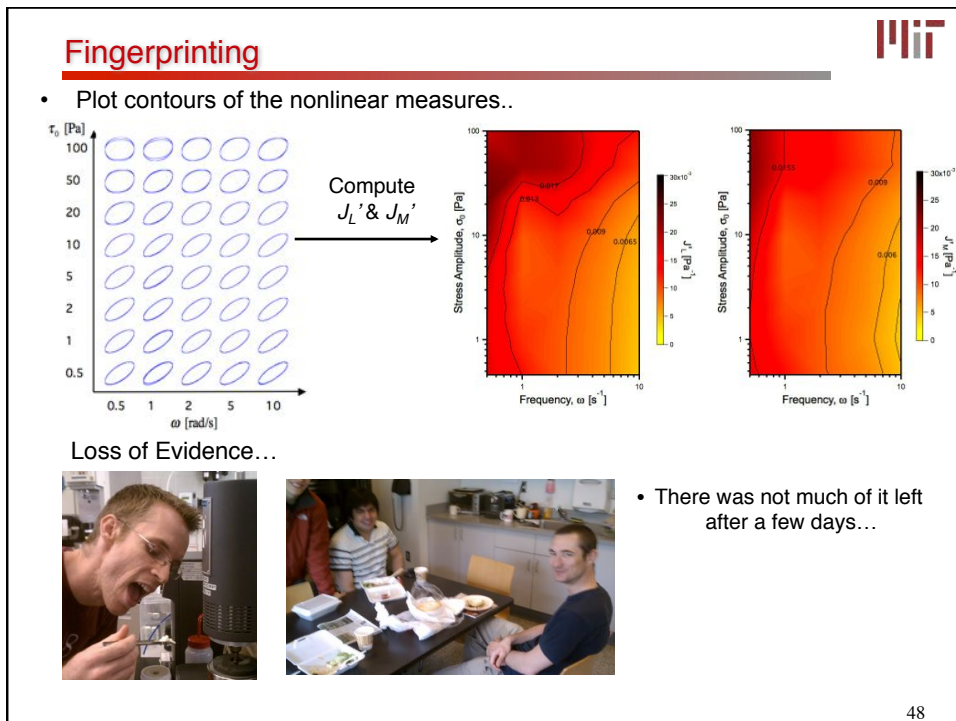
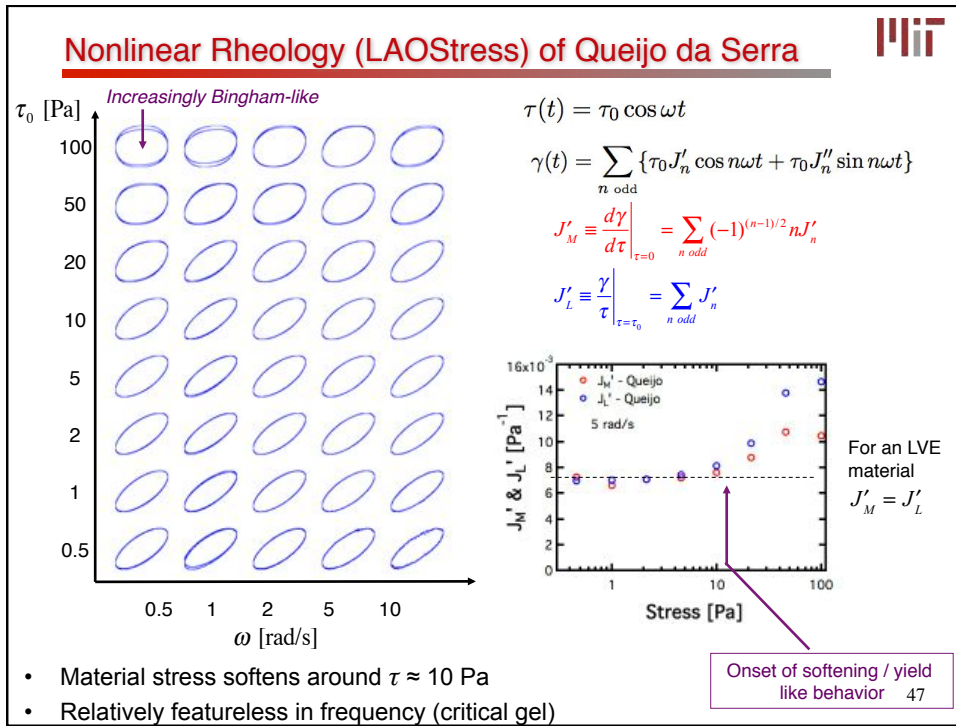



$G^* = \Gamma(n) S \omega^n$
 $n \approx \frac{1}{2}$

- Cheese: the famous “Queijo da Serra”
- LVE: Very close to a critical gel with $G' = G''$
- What about the nonlinear behavior?
- Use LAOStress to study it...

Fractional Calculus for Power-Law Gels
 K. Song et al. *Korea-Aust Rheol. Journal*, **18** (2006)
 A. Jaishankar & GHM, *Proc. Roy. Soc. A* (2012), in press

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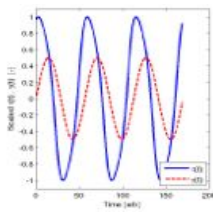




Summary of Rheological Fingerprinting

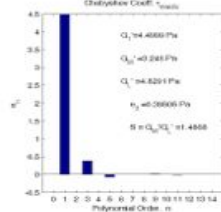
- A physical interpretation and language for LAOS experiments in complex fluids
- Framework of elastic/viscous stress decomposition plus **Chebyshev coefficients**

Time Series



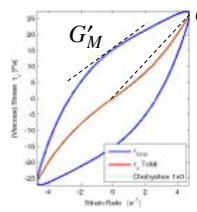
$T_n(\gamma) = \cos(n\omega t)$
 $\dot{\gamma} = \frac{\dot{\gamma}(t)}{\gamma_0 \omega}$

Harmonic Coefficients



$$\tau(t; \omega, \gamma_0) \equiv \tau_{elastic}(\gamma(t)) + \tau_{viscous}(\dot{\gamma}(t)) = \gamma_0 \sum_{i=1}^N e_i T_i(x) + \gamma_0 \omega \sum_{i=1}^N v_i T_i(y)$$

Bowditch-Lissajous Figures



Measures of Nonlinearity

$$G'_M = \left. \frac{d\tau}{d\gamma} \right|_{\gamma=0} = e_1 - 3e_3 + 5e_5 + \dots$$

$$G'_L = \left. \frac{\tau}{\gamma} \right|_{\gamma=\gamma_0} = e_1 + e_3 + e_5 + \dots$$


$$S = \frac{G'_L - G'_M}{G'_L}$$

$$T = \frac{\eta'_L - \eta'_M}{\eta'_L}$$

- Also applicable to thixotropic and 'yield stress' responses: *elasto-visco-plastic* materials
Ewoldt, et al. *Rheol. Acta*, 49(2), 2010; Dimitriou, Ewoldt, GHM, *J. Rheol.* In prep

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SAOS
MAOS
LAOS_{Strain}, LAOS_{Stress}
....what's next....?



Perhaps: Complete Harmonic Analysis of Oscillating Shear ??

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- Jeff Giacomin (Wisconsin)
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- Dimitris Vlassopoulos (FORTH)




MIT Hooding, 2009


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- Chevron Energy Technology Corp.
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- Schlumberger Foundation
- National Science Foundation



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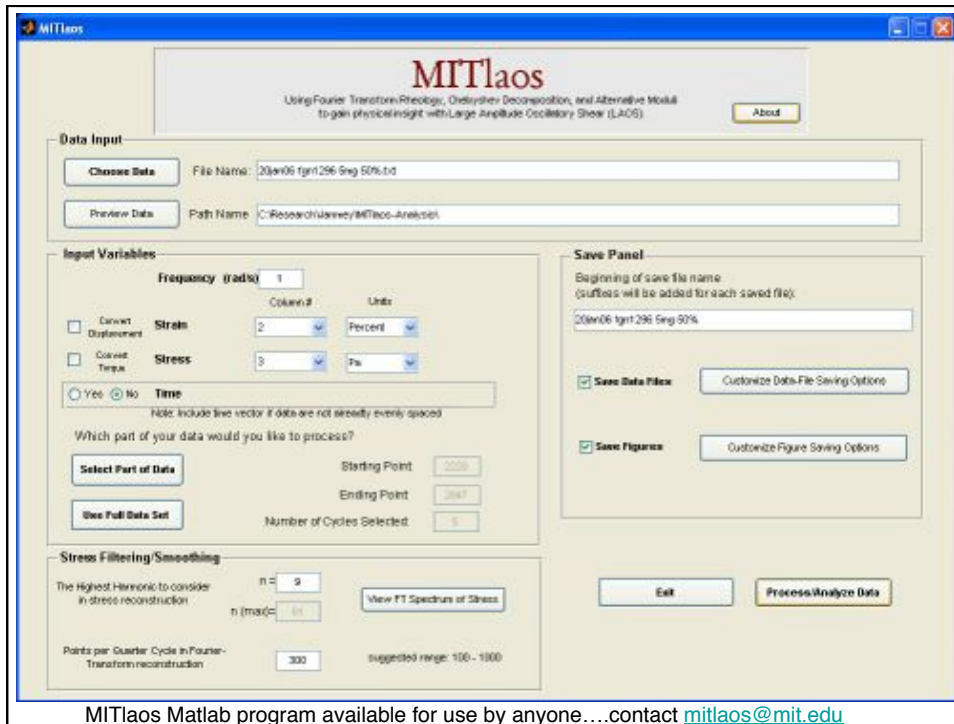
Chris Dimitriou

Randy Ewoldt

Thomas Ober

Laura Casanellas

12:45 am Lisbon, Aug 10, 2012!



MITlaos Matlab program available for use by anyone....contact mitlaos@mit.edu

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