

Notes on  
**1.63 Advanced Environmental Fluid Mechanics**  
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## 3.10 Oscillatory Boundary Layers

### 3.10.1 Stokes problem

If the viscosity is weak or the frequency is high (time scale is small), there is a boundary layer near the boundary of an oscillating body or the solid bottom under a wave.

Let the external flow have the tangential velocity  $u = \Re U(x)e^{-i\omega t}$ . If the inertia parameter is small, then

$$\frac{uu_x, vu_y}{u_t} = O\left(\frac{U_o}{\omega L}\right) \ll 1.$$

If furthermore

$$1 \gg \frac{U}{\omega L} \gg \frac{\nu}{\omega L^2}$$

we keep just the most important viscous stress term and seek perturbation solution in successive powers of the inertia parameter. Let us save the trouble of nondimensionalization and assume

$$u = u_1 + u_2 + \dots \quad (3.10.1)$$

with the understanding that the relative orders of magnitude is represented by the subscripts, i.e.,  $u_1$  is the leading order and  $u_2$  is smaller than  $u_1$  by a factor  $O(\frac{U}{\omega L} \gg \frac{\nu}{\omega L^2})$ , etc. We get from the Navier-Stokes equations the leading order approximation

$$\frac{\partial u_1}{\partial t} = \frac{\partial}{\partial t} \text{Re} (Ue^{-i\omega t}) + \nu \frac{\partial^2 u_1}{\partial y^2} \quad y > 0 \quad (3.10.2)$$

subject to the boundary conditions that

$$u_1 \rightarrow \text{Re} Ue^{-i\omega t} \quad y \rightarrow \infty \quad (3.10.3)$$

and

$$u_1 = 0 \quad y = 0 \quad (3.10.4)$$

Let

$$u_1 = \text{Re} [\hat{u}_1(x, y)e^{-i\omega t} + Ue^{-i\omega t}] \quad (3.10.5)$$

then

$$-i\omega U - i\omega \hat{u}_1 = -i\omega U + \nu \frac{d^2 \hat{u}_1}{dy^2}$$

Therefore,

$$\frac{d^2 \hat{u}_1}{dy^2} + \frac{i\omega}{\nu} \hat{u}_1 = 0 \quad (3.10.6)$$

$$\hat{u}_1 \rightarrow 0, \quad y \rightarrow \infty \quad (3.10.7)$$

$$\hat{u}_1 = -U_1(x), \quad y = 0 \quad (3.10.8)$$

The solution is

$$\hat{u}_1 = -U(x) \exp \left[ -(1-i)y \sqrt{\frac{\omega}{2\nu}} \right] \quad (3.10.9)$$

or,

$$u_1 = \Re \left\{ U(x) \left[ 1 - \exp \left( -(1-i)y \sqrt{\frac{\omega}{2\nu}} \right) \right] e^{-i\omega t} \right\} \quad (3.10.10)$$

The sign of  $\sqrt{-i}$  is chosen so that (3.10.7) is satisfied. The boundary layer thickness is

$$\delta = \sqrt{\frac{2\nu}{\omega}} \quad (3.10.11)$$

It is easy to show that the vorticity at the wall is

$$-\left. \frac{\partial u_1}{\partial y} \right|_{y=0} = (1-i)U \sqrt{\frac{\omega}{2\nu}} = e^{-i\pi/4} U \quad (3.10.12)$$

which has the phase lag of  $\pi/4$  behind  $U$ , and diffuses away from  $y = 0$  like a propagating wave exponentially attenuated after the Stokes boundary layer thickness  $O(\delta)$ .

### 3.10.2 Induced Streaming

By considering the small effect of convective inertia, the second order improvement is physically even more interesting.

If the inviscid outer flow has tangential variation  $\frac{dU}{dx} \neq 0$ , then by continuity there is transverse flow  $v_1$  in the boundary layer :

$$\begin{aligned} v_1 &= -\int_0^y \frac{\partial u_1}{\partial x} dy = ie^{-i\omega t} \frac{dU}{dx} \int_0^y \left[ 1 - e^{-(1-i)y/\delta} \right] dy \\ &= -e^{-i\omega t} \frac{dU}{dx} \left\{ y - \frac{\delta}{1-i} \left[ 1 - e^{-(1-i)y/\delta} \right] \right\} \end{aligned} \quad (3.10.13)$$

which is valid in  $y \leq O(\delta)$  only.

Let us examine the second order:

$$\begin{aligned} \frac{\partial u_2}{\partial t} - \nu \frac{\partial^2 u_2}{\partial y^2} &= U \frac{dU}{dx} - \left( u_1 \frac{\partial u_1}{\partial x} + v_1 \frac{\partial u_1}{\partial y} \right) \\ &= U \frac{dU}{dx} - \left[ \frac{\partial (u_1 u_1)}{\partial x} + \frac{\partial (u_1 v_1)}{\partial y} \right] \end{aligned}$$

Taking average over a period

$$-\nu \frac{\partial^2 \bar{u}_2}{\partial y^2} = U \frac{dU}{dx} - \left( \overline{\frac{\partial u_1 u_1}{\partial x}} + \overline{\frac{\partial u_1 v_1}{\partial y}} \right)$$

On the right-hand-side the last two terms  $\overline{u_1 u_1}$ ,  $\overline{u_1 v_1}$  are wave-induced Reynolds stresses

$\overline{u_1 u_1}$  = rate of transporting  $x$ -momentum in  $x$ -direction

$\overline{u_1 v_1}$  = rate of transporting  $x$ -momentum in  $y$ -direction

Alternatively:

$$-\nu \frac{\partial^2 \bar{u}_2}{\partial y^2} = \frac{1}{2} \frac{\partial}{\partial x} \overline{U^2} - \frac{1}{2} \frac{\partial}{\partial x} \overline{u_1^2} - v_1 \frac{\partial u_1}{\partial y}$$

Let

$$\alpha = (1 - i)/\delta \quad (3.10.14)$$

Since

$$v_1 = ie^{-i\omega t} \frac{1}{\alpha} \frac{dU}{dx} (\alpha y - 1 + e^{-\alpha y})$$

$$\frac{\partial u_1}{\partial y} = \alpha U(x) e^{-i\omega t} e^{-\alpha y}$$

$$\overline{v_1 \frac{\partial u_1}{\partial y}} = \frac{1}{2} \text{Re} \left[ U^* \frac{dU}{dx} \frac{\alpha^*}{\alpha} e^{-\alpha^* y} (\alpha y - 1 + e^{-\alpha y}) \right]$$

Thus

$$\begin{aligned} -\nu \frac{\partial^2 \bar{u}_2}{\partial y^2} &= G(y) \equiv \frac{1}{2} \frac{d|U|^2}{dx} \left[ 1 - (1 - e^{-\alpha y}) (1 - e^{-\alpha^* y}) \right] \\ &\quad + \text{Re} U^* \frac{dU}{dx} \frac{\alpha^*}{\alpha} e^{-\alpha^* y} (\alpha y - 1 + e^{-\alpha y}) \\ \nu \frac{\partial \bar{u}_2}{\partial y} &= \int_y^\infty G(y') dy' \\ \nu \bar{u}_2 &= \int_0^y dy'' \int_{y''}^\infty G(y') dy' \\ &= -y \int_y^\infty G(y') dy' + \int_0^y y'' G(y'') dy'' \end{aligned}$$

One more integration gives

$$\begin{aligned} -\omega \bar{u}_2 &= \text{Re} F_4 U \frac{dU^*}{dx}. \quad \text{where} \\ F_4 &= -\frac{1}{2} (1 - 3i) e^{-(1-i)\eta} - \frac{i}{2} e^{-(1+i)\eta} - \frac{1}{4} (1 + i) e^{-2\eta} \\ &\quad + \frac{1}{2} (1 + i) \eta e^{-(1-i)\eta} + \frac{3}{4} (1 - i) \end{aligned}$$

Note that as  $y \rightarrow \infty$ , just outside the boundary layer,

$$\bar{u}_2 = -\frac{1}{4\omega} \text{Re} \left[ (3-i) U \frac{dU^*}{dx} \right]$$

Let  $U = Ae^{i\gamma}$

$$U \frac{dU^*}{dx} = Ae^{i\gamma} \frac{dAe^{-i\gamma}}{dx} = \frac{dA^2/2}{dx} - iA^2 \frac{d\gamma}{dx}$$

Hence

$$\bar{u}_2(\infty) = -\frac{1}{4\omega} \left( \frac{3}{2} \frac{dA^2}{dx} - 3A^2 \frac{d\gamma}{dx} \right) \quad (3.10.15)$$

Example: Progressive waves,  $U = U_0 e^{ikx}$ , where  $U_0, k$  are constants

$$\bar{u}_2(\infty) = \frac{3k}{4\omega} U_0^2 \quad (3.10.16)$$

### 3.10.3 Physics of the Induced Streaming

Take a progressive water waves as an example:

Outside the B.L. :

$$u_\infty = A \cos(\omega t - kx) \quad (3.10.17)$$

Inside the B.L.

$$u = A \left[ \cos(\omega t - kx) - e^{-y/\delta} \cos(\omega t - kx - y/\delta) \right] \quad (3.10.18)$$

where the velocity amplitude  $A$  is related to the surface amplitude "a" by

$$A = a\omega / \sin kh \quad (3.10.19)$$

Let's find the induced transverse velocity  $v$

$$\begin{aligned} \frac{\partial u}{\partial x} &= A \sin(\omega t - kx) - Ae^{-y/\delta} \sin(\omega t - kx - y/\delta) \\ v_\infty &= -\int_0^{y \gg \delta} \frac{\partial u}{\partial x} dy = -y A \sin(\omega t - kx) - \frac{1}{2} Ak\delta \cos(\omega t - kx) + \frac{1}{2} Ak\delta \sin(\omega t - kx) \end{aligned}$$

Now

$$\overline{u_\infty v_\infty} = -\frac{1}{4} A^2 k\delta < 0$$

where the  $\sin(\omega t - kx)$  terms in  $v_\infty$  are out of phase with  $u_\infty$  by  $\pi/2$ , hence does not contribute to the mean.

Now consider a slice of boundary layer one wavelength long. Because of periodicity, there is no net transfer of momentum or forces at two ends  $x_0$  and  $x_0 + 2\pi/k$ . But the momentum transfer downwards is  $\frac{A^2}{4} k\delta$ , causing a positive shear stress. To balance it there must be a non-zero  $\mu \frac{\partial \bar{u}}{\partial y}$  at all levels  $y$  below the top. Hence,  $\bar{u} \neq 0$ , resulting in induced streaming.

**Homework:** Find the induced streaming in Stokes boundary layer under a standing wave with

$$U(x) = A \cos kx e^{-i\omega t}.$$

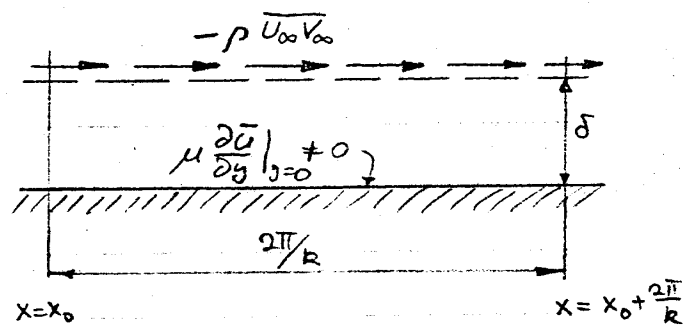


Figure 3.10.1: Reynolds stress and Induced streaming in Stokes layer