

**Lecture notes in Fluid Dynamics**

(1.63J/2.01J)

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4-4 buoyplum.tex

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## 4.4 Buoyant plume from a steady heat source

[Reference]: Gebhart, et. al. (Jalluria, Maharjan, Saammakia), **Buoyancy-induced Flows and Transport**, 1988, Hemisphere Publishing Corporation

Let  $\tilde{T} = T - T_\infty =$  temperature variation where  $T_\infty$  is a constant (no ambient stratification). For a strong enough heat source, we expect the boundary layer behavior,

$$\frac{\partial}{\partial r} \gg \frac{\partial}{\partial x}, \quad u \gg v, \quad \frac{\partial p}{\partial r} \cong 0$$

The boundary layer equations are

$$\frac{\partial(ru)}{\partial x} + \frac{\partial(rv)}{\partial r} = 0 \tag{4.4.1}$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial r} = g\beta(T - T_\infty) + \frac{\nu}{r} \frac{\partial}{\partial r} \left( r \frac{\partial u}{\partial r} \right) \tag{4.4.2}$$

$$u \frac{\partial \tilde{T}}{\partial x} + v \frac{\partial \tilde{T}}{\partial r} = \frac{k}{r} \frac{\partial}{\partial r} \left( r \frac{\partial \tilde{T}}{\partial r} \right) \tag{4.4.3}$$

The centerline  $r = 0$  is an axis of symmetry,

$$v = \frac{\partial u}{\partial r} = \frac{\partial \tilde{T}}{\partial r} = 0 \tag{4.4.4}$$

Far outside the plume  $r \rightarrow \infty$

$$u \rightarrow 0 \text{ and } T \rightarrow T_\infty, (\tilde{T} \rightarrow 0) \tag{4.4.5}$$

Rewrite (4.4.3) as

$$\begin{aligned} & \frac{\partial(ru\tilde{T})}{\partial x} + \frac{\partial(rv\tilde{T})}{\partial r} - \tilde{T} \left( \frac{\partial(ru)}{\partial x} + \frac{\partial(rv)}{\partial r} \right) \\ & = \frac{\partial(ru\tilde{T})}{\partial x} + \frac{\partial(rv\tilde{T})}{\partial r} = k \frac{\partial}{\partial r} \left( r \frac{\partial \tilde{T}}{\partial r} \right) \end{aligned} \tag{4.4.6}$$

after using continuity. Now integrating the last equation from  $r = 0$  to  $r = \infty$

$$\begin{aligned} \frac{\partial}{\partial x} \int_0^\infty 2\pi r u \tilde{T} dr + 2\pi \int_0^\infty \frac{\partial(rv\tilde{T})}{\partial r} dr \\ = k2\pi \int_0^\infty dr \frac{\partial}{\partial r} \left( r \frac{\partial \tilde{T}}{\partial r} \right) \end{aligned}$$

therefore

$$\frac{\partial}{\partial x} \int_0^\infty 2\pi r u \tilde{T} dr + 2\pi r v \tilde{T} \Big|_0^\infty = 2\pi k \left( r \frac{\partial \tilde{T}}{\partial r} \right)_{r=0}^{r=\infty} \quad (4.4.7)$$

Using the boundary conditions, we get or

$$\int_0^\infty 2\pi r u \tilde{T} dr = \text{constant}$$

Note that

$$\begin{aligned} \int_0^\infty 2\pi r dr u \rho C \tilde{T} &= \text{rate of buoyancy flux} \\ &= \text{rate of heat flux} \\ &= Q(\text{given rate of heat release at } x = 0) \end{aligned}$$

therefore,

$$Q = \int_0^\infty 2\pi r dr \rho u C \tilde{T} \quad (4.4.8)$$

This is a boundary condition.

Let the stream function  $\psi$  be defined by

$$ru = \frac{\partial \psi}{\partial r}, \quad rv = -\frac{\partial \psi}{\partial x} \quad (4.4.9)$$

(4.4.1) is automatically satisfied. From the momentum equation:

$$\left( \frac{1}{r} \frac{\partial \psi}{\partial r} \right) \frac{1}{r} \frac{\partial^2 \psi}{\partial x \partial r} - \frac{1}{r} \frac{\partial \psi}{\partial x} \frac{\partial}{\partial r} \left( \frac{1}{r} \frac{\partial \psi}{\partial r} \right) = g\beta \tilde{T} + \frac{\nu}{r} \frac{\partial}{\partial r} \left[ r \frac{\partial}{\partial r} \left( \frac{1}{r} \frac{\partial \psi}{\partial r} \right) \right] \quad (4.4.10)$$

From the energy equation

$$\frac{1}{r} \frac{\partial \psi}{\partial r} \frac{\partial \tilde{T}}{\partial x} - \frac{1}{r} \frac{\partial \psi}{\partial x} \frac{\partial \tilde{T}}{\partial r} = \frac{k}{r} \frac{\partial}{\partial r} \left( r \frac{\partial \tilde{T}}{\partial r} \right) \quad (4.4.11)$$

and from the buoyancy flux condition

$$Q = 2\pi \rho C \int_0^\infty r dr \left( \frac{1}{r} \frac{\partial \psi}{\partial r} \right) \tilde{T} \quad (4.4.12)$$

Try a similarity solution with the one-parameter transformation

$$x = \lambda^a x^*, \quad r = \lambda^b r^*, \quad \psi = \lambda^c \psi^*, \quad \tilde{T} = \lambda^d T^*$$

From (4.4.10),

$$\lambda^{2c-4b-a} = \lambda^{2c-4b-a} = \lambda^d = \lambda^{c-4b} \quad (4.4.13)$$

from (4.4.11)

$$\lambda^{c+d-2b-a} = \lambda^{d-2b} \quad (4.4.14)$$

and from (4.4.12)

$$\lambda^{c+d} = 1 \quad (4.4.15)$$

From these three equations we get

$$\frac{c}{a} = 1, \quad \frac{b}{a} = \frac{1}{2}, \quad \frac{d}{a} = -1.$$

We leave it as an exercise to show that the similarity variable can be taken to be

$$\eta = \frac{r}{x^{1/2}} \quad (4.4.16)$$

and the similarity solutions to be

$$\psi = xF(\eta), \quad \text{and} \quad \tilde{T} = x^{-1}G(\eta) \quad (4.4.17)$$

After much algebra, and noting

$$\frac{\partial \eta}{\partial r} = \frac{1}{x^{1/2}}, \quad \frac{\partial \eta}{\partial x} = -\frac{1}{2} \frac{r}{x^{3/2}} = -\frac{1}{2} \frac{r}{x^{1/2}} \frac{1}{x} = -\frac{\eta}{2x}$$

we get from (4.4.10)

$$\nu F''' + \left( \frac{F'}{\eta} \right)' (F - \nu) + g\beta\eta G = 0 \quad (4.4.18)$$

and from (4.4.11)

$$k(\eta G')' + (FG)' = 0 \quad (4.4.19)$$

Before integrating, let us normalize :

$$\eta = \alpha \bar{\eta}, \quad F = \gamma \bar{F}, \quad G = \sigma \bar{G}. \quad (4.4.20)$$

It follows from (4.4.18) that

$$\frac{\nu\gamma}{\alpha^3} \bar{F}''' + \frac{\gamma}{\alpha^3} \left( \frac{\bar{F}'}{\bar{\eta}} \right)' (\gamma \bar{F} - \nu) + g\beta\alpha\sigma\bar{\eta}\bar{G} = 0 \quad (4.4.21)$$

where prime denotes  $d/d\bar{\eta}$ . Setting  $\gamma = \nu$  and

$$\frac{\nu^2}{\alpha^3} = g\beta\alpha\sigma$$

which relates  $\sigma$  and  $\alpha$ ,

$$\sigma = \frac{\nu^2}{g\beta\alpha^4} \quad (4.4.22)$$

we get

$$\bar{F}'''' + \left(\frac{\bar{F}'}{\bar{\eta}}\right)' (\bar{F} - 1) + \bar{\eta}\bar{G} = 0 \quad (4.4.23)$$

Similar normalization of (4.4.19) gives

$$\frac{k\alpha\sigma}{\alpha^2}(\bar{\eta}\bar{G}')' + \frac{\gamma\sigma}{\alpha}(\bar{F}\bar{G})' = 0 \quad (4.4.24)$$

. which can be simplified to

$$(\bar{\eta}\bar{G}')' + P_r(\bar{F}\bar{G})' = 0 \quad (4.4.25)$$

. where

$$P_r = \frac{\nu}{k} = \text{Prandtl Number} \quad (4.4.26)$$

For water  $\nu = 10^{-2}cm^2/s, k = 1.42cm^2/s$ , hence  $Pr = 7$ . For air  $\nu = 0.145cm^2/s, k = 0.202cm^2/s$ , hence  $Pr = 0.75$ .

We now integrate (4.4.25) to give

$$\bar{\eta}\bar{G}' + P_r\bar{F}\bar{G} = \text{constant}$$

Since  $\psi(x, 0) = 0$ , we must have  $\bar{F}(0) = 0$ ; the constant above is zero.

$$\bar{\eta}\bar{G}' + P_r\bar{F}\bar{G} = 0 \quad (4.4.27)$$

Equation (4.4.27) can be written

$$\begin{aligned} \frac{\bar{G}'}{\bar{G}} &= -P_r\frac{\bar{F}}{\bar{\eta}}, \quad \text{or} \quad \frac{d \ln \bar{G}}{d\bar{\eta}} = -P_r\frac{\bar{F}}{\bar{\eta}} \\ \ln \bar{G} &= -P_r \int_0^{\bar{\eta}} \frac{\bar{F}}{\bar{\eta}} d\bar{\eta} + \text{constant} \\ \bar{G}(\bar{\eta}) &= \bar{G}(0) \exp\left(-P_r \int_0^{\bar{\eta}} \frac{\bar{F}}{\bar{\eta}} d\bar{\eta}\right) \end{aligned} \quad (4.4.28)$$

Substituting Eqn. (4.4.28) into Eqn. (4.4.23), the resulting equation for  $\bar{F}$  must be integrated numerically.

Now let us find the boundary conditions for  $F$  or  $\bar{F}$ .

Eqn. (4.4.8 ) becomes

$$\frac{Q}{2\pi\rho C} = \int_0^\infty dr r \left( \frac{1}{r} \frac{\partial\psi}{\partial r} \right) \frac{G(\eta)}{x} = \int_0^\infty dr \frac{r}{r} x^{1/2} F' \frac{G}{x} = \int_0^\infty d\eta (F'G) = \nu\sigma \int_0^\infty d\bar{\eta} (\bar{F}'\bar{G}) \quad (4.4.29)$$

Therefore,

$$\int_0^\infty d\bar{\eta} \bar{F}'\bar{G} = \frac{Q}{2\pi\rho C\nu\sigma} \quad (4.4.30)$$

Let us choose

$$\frac{Q}{2\pi\rho C\nu\sigma} = 1 \quad (4.4.31)$$

so that

$$\int_0^\infty d\bar{\eta} \bar{F}'\bar{G} = 1 \quad (4.4.32)$$

is the boundary condition for  $\bar{F}$  and  $\bar{G}$ . Now (4.4.31) defines  $\sigma$ , the scale of  $G$ . Note that larger  $Q$  implies larger  $\sigma$  and smaller  $\alpha$ . Thus a stronger heat source leads to a greater centerline temperature and a thinner plume. Also,

$$u \rightarrow 0 \quad \text{as } r \rightarrow \infty$$

hence

$$u = \frac{1}{r} \psi_r = \frac{F'}{\eta} = \frac{\nu}{\alpha^2} \frac{\bar{F}'}{\bar{\eta}} \rightarrow 0, \quad \text{as } \eta \sim \bar{\eta} \rightarrow \infty$$

The radial velocity is, in general

$$v = \frac{1}{r} \psi_x = \frac{1}{r} \left( F - \eta \frac{F'}{2} \right)$$

Since

$$v \rightarrow 0 \quad \text{as } \eta \rightarrow 0,$$

we must have,

$$F(0) = 0.$$

Clearly

$$\bar{F}(\bar{\eta}) = 0 \quad \text{as } \bar{\eta} \rightarrow 0 \quad (4.4.33)$$

The numerical results by Mollendorf & Gelhart, 1974, are shown in Figs. 4.4.1, for various Prandtl numbers. A schlieren photograph due to Gebhart (copied from Van Dyke **An Album of Fluid Motion**) is shown in Figure fig:plumeVD.

Remark:

$$u = \frac{1}{r} \frac{\partial\psi}{\partial r} = \frac{F'}{\eta} \left( = \frac{x}{r} F' \frac{1}{x^{1/2}} \right)$$

Along the centerline  $u(x, 0) = \left( \frac{F'}{\eta} \right)_0 = \text{constant}$  depending on  $P_r$ . Why? Buoyancy acceleration is counteracted by entrainment.

Remark: Let the radius of the plume be  $a$  which varies as

$$a \sim x^{1/2}$$

This is consistent with the behavior that  $u \sim x^0$ , and  $\tilde{T} \sim x^{-1}$ , since

$$a^2 u \tilde{T} = Q$$

On the other hand the mass flux rate is

$$u a^2 \sim x$$

and the momentum flux rate is

$$u^2 a^2 \sim x$$

hence both approach zero at the source. Thus a plume is the result of energy source, not of mass or momentum.

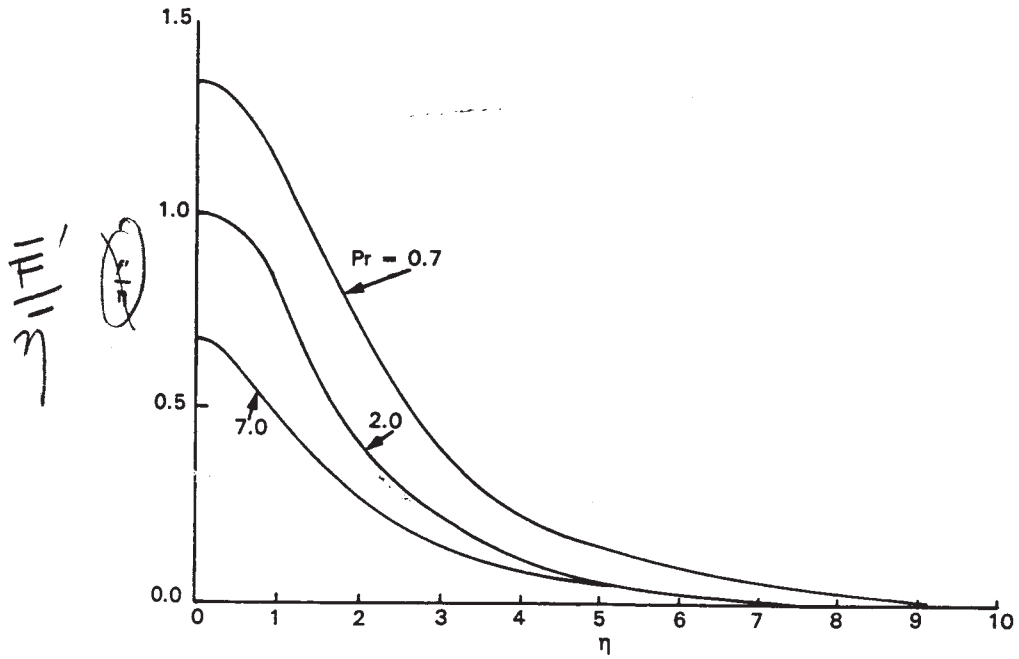


Figure 4.4.1 Velocity profiles in an axisymmetric plume. (From Mollendorf and Gebhart, 1974.)

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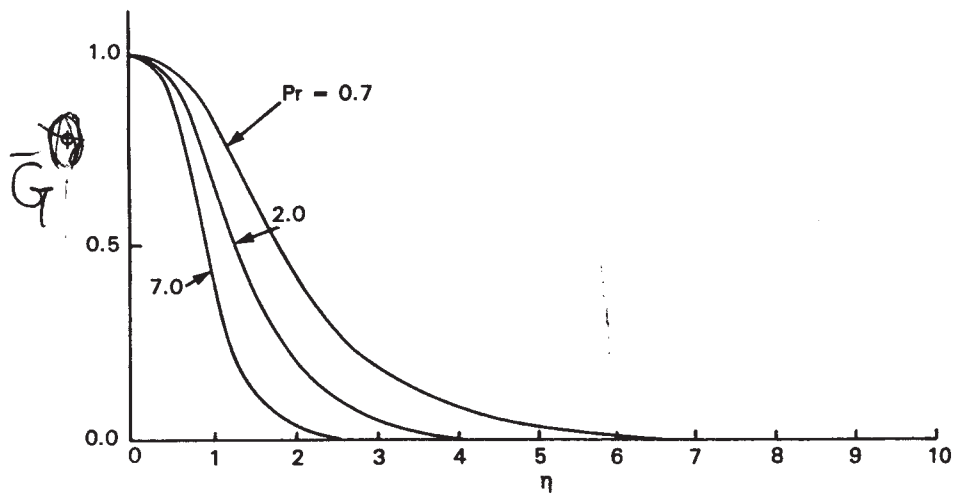


Figure 4.4.2 Temperature profiles in an axisymmetric plume. (From Mollendorf and Gebhart, 1974.)

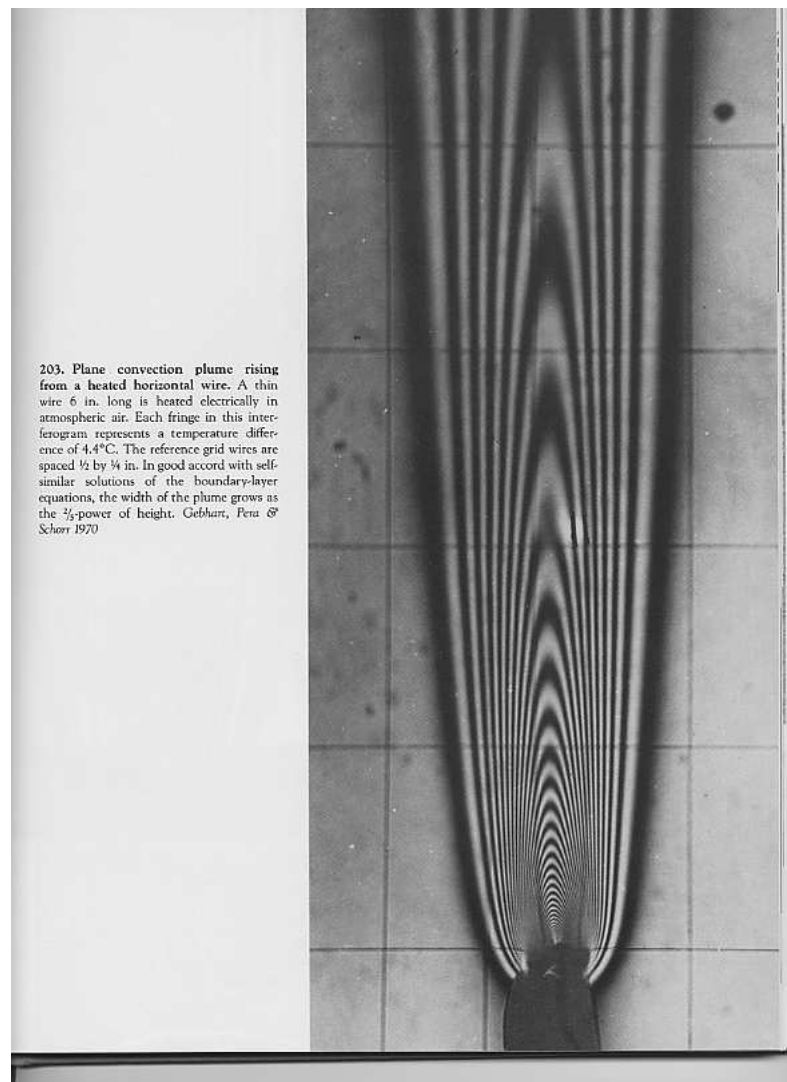


Figure 4.4.2: A 2D thermal plume from a line heat source. From Van Dyke, photo by Gebhart, Pera and Schorr 1970,